



Course Outline

- Basics in Rheology Theory
- TA Instruments Rheometers
 - Instrumentation
 - Choosing a Geometry
- Rheology Experimental
 - Flow tests
 - Oscillation tests
 - Transient tests
- Applications of Rheology
 - Polymers
 - Yield stress and thixotropy of structured fluids



Basics in Rheology Theory



Rheology: An Introduction











Rheology: The study of the flow and deformation of matter. Rheological behavior affects every aspect of our lives.





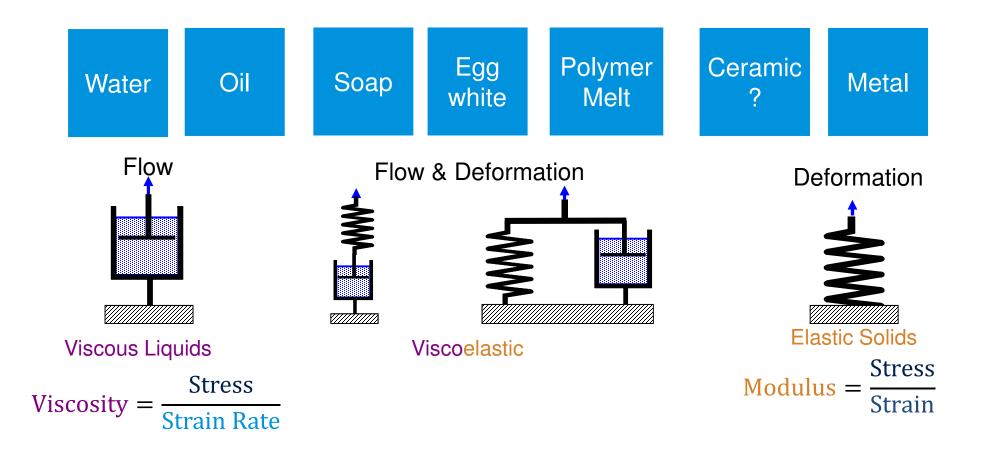








Basic Material Behaviors

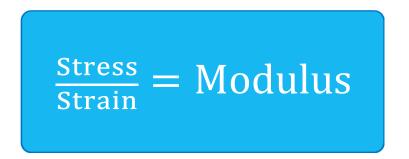




Rheology: An Introduction

- Rheology is the study of flow and deformation of matter
 - The word 'Rheology' was coined in the 1920s by Professor E C Bingham at Lafayette College
- Flow is a special case of deformation
- The relationship between stress and deformation is a property of the material



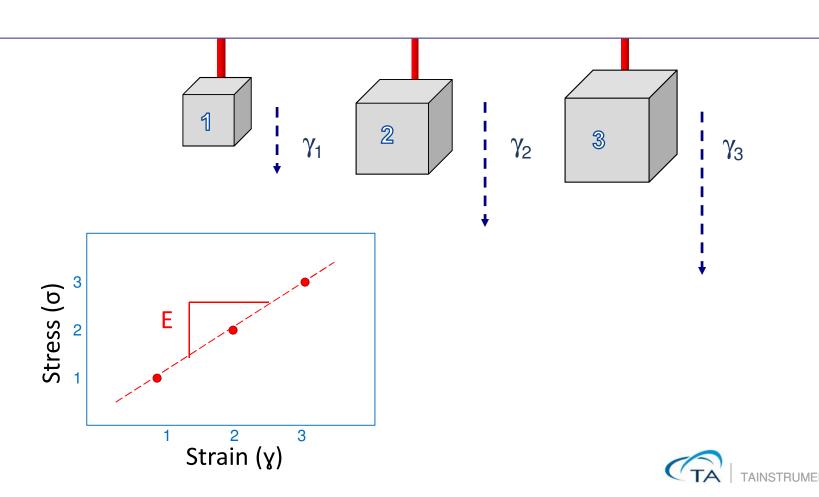




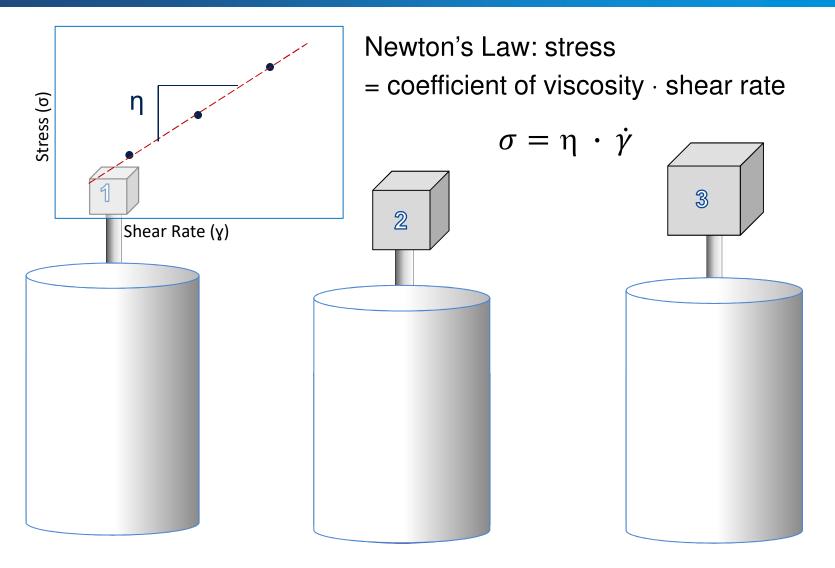
Elastic Behavior of an Ideal Solid

Hooke's Law of Elasticity: Stress = Modulus · Strain

$$\sigma = E \cdot \gamma$$



Viscous Behavior of an Ideal Liquid





Viscoelasticity Defined

Range of Material Behavior Liquid Like----- Solid Like Ideal Fluid ----- Most Materials -----Ideal Solid Purely Viscous ----- Viscoelastic ----- Purely Elastic

Viscoelasticity: Having both viscous and elastic properties

 Materials behave in the linear manner, as described by Hooke and Newton, only on a small scale in stress or deformation.



Solid or Liquid?



- Long deformation time: pitch behaves like a highly viscous liquid
 - 9th drop fell July 2013
- Short deformation time: pitch behaves like a solid

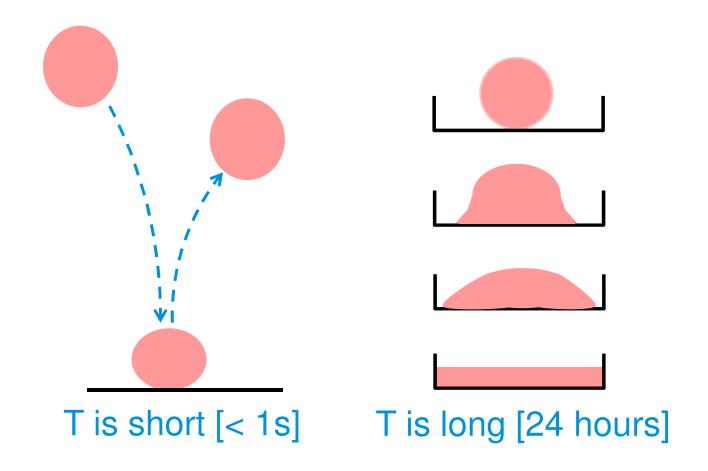


Started in 1927 by Thomas Parnell in Queensland, Australia

http://www.theatlantic.com/technology/archive/2013/07/the-3-most-exciting-words-in-science-right-now-the-pitch-dropped/277919/



Time-Dependent Viscoelastic Behavior





Importance of Rheological Measurements

- Investigating molecular structure
- Guide and troubleshooting processing
- Evaluate product performance



viscoelastic properties



Basic Parameters and Units

```
Stress = Force /Area [Pa, or dyne/cm<sup>2</sup>]
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\sigma = shear stress
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Strain = Geometric Shape Change [no units]

 γ = shear strain

Strain Rate or Shear Rate = Velocity Gradient [1/s]

 $\dot{\gamma}$ = shear strain rate

Modulus = Stress / Strain [Pa or dyne/cm²]

G = Shear Modulus

Compliance = Strain / Stress [1/Pa or cm²/dyne]

Typically denoted by J

Viscosity = Stress /Strain Rate [Pa·s or Poise]

Denoted by $\boldsymbol{\eta}$

S.I. units × 10 *= c.g.s. units*



TA Instruments Rheometers



Types of Rheometers

- Rotational (Shear) Rheometers
 - ARES-G2 and ARES (Strain Control SMT)
 - DHR or AR (Stress Control CMT)

Closed Die Cavity Rheometer (Strain Control – SMT)

- Solids (Tensile/Bending) Rheometers
 - RSA-G2 and RSA (Strain Control SMT)
 - DMA 850/Q800 (Stress Control CMT)

SMT: <u>Separate</u> Motor and Transducer (Dual-Head) **CMT:** <u>Combined</u> Motor and Transducer (Single Head)



Rotational Rheometers by TA

ARES G2



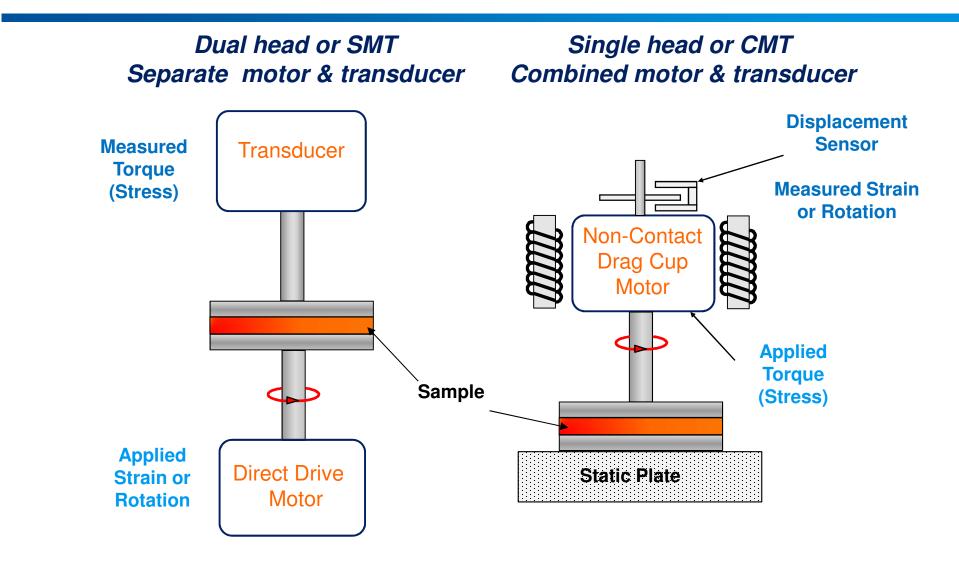
Controlled Strain Dual Head SMT DHR



Controlled Stress Single Head CMT



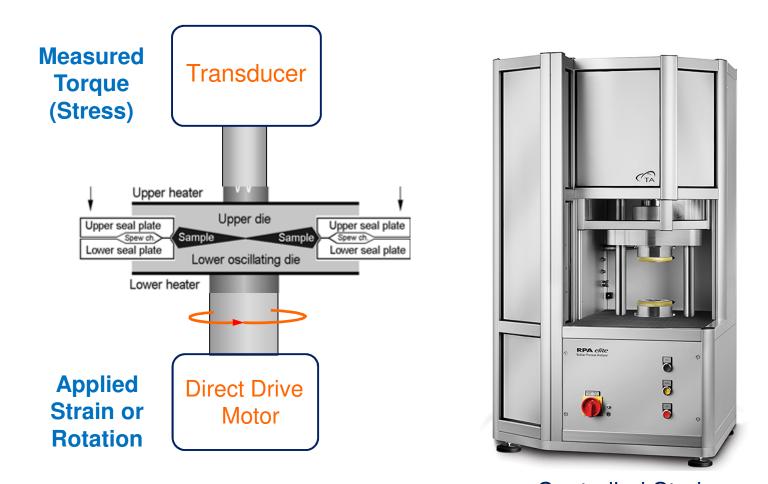
Rotational Rheometer Designs



Note: With computer feedback, DHR and AR can work in controlled strain/shear rate, and ARES can work in controlled stress.



Closed Die Cavity Rheometer by TA

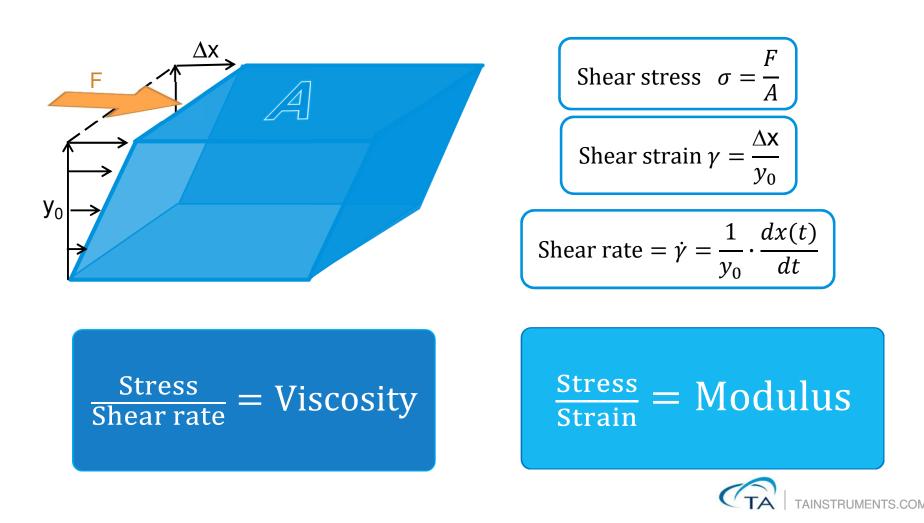


RPA Elite, RPA Flex and MDR SMT or Dual Head



How do Rheometers Work?

The study of <u>stress</u> and <u>deformation</u> relationship



How do Rheometers Work?

- In a rheological measurement, stress; strain and strain rate (shear rate) are all calculated signals
- The raw signals behind the scene are torque; angular displacement and angular velocity

Fundamentally, a rotational rheometer will apply or measure:

- Torque (Force)
 Angular Displacement
 - 3. Angular Velocity



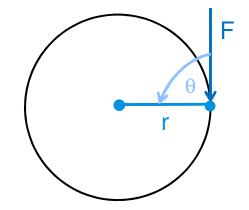
Measured parameter: torque

•Torque (M) is a measure of how much a force (F) acting on an object causes that object to rotate.

- The object rotates about an axis, called the pivot point
- The distance (r) from the pivot point to the point where the force acts is called the moment arm
- The angle (θ) at which the force acts at the moment arm

$$M = r \cdot F \cdot \sin \theta = r \cdot F$$

(for $\theta = 90^{\circ}$ as shown)





Calculated parameter: stress

•Shear stress is calculated from the torque and geometry stress constant

$\sigma = M \cdot K_{\sigma}$

- • σ = shear stress (Pa or Dyne/cm²)
- M = torque (N·m or gm·cm)
- • K_{σ} = stress constant
- The stress constant, K_{σ} , is dependent on measurement geometry and/or initial sample dimensions

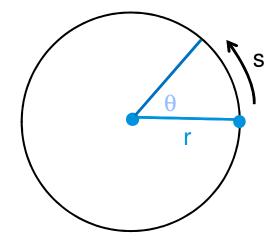


Measured parameter: angular displacement

•Angular displacement (θ) is the angle, in radians, through which an object moves on a circular path

- •s = arc length (or linear displacement)
- r = radius of a circle
 - Conversion: degrees = radians $\cdot 180/\pi$

$$\theta = s/r$$





Calculated parameter: strain

•Strain is a measure of deformation representing the angular displacement relative to a reference length

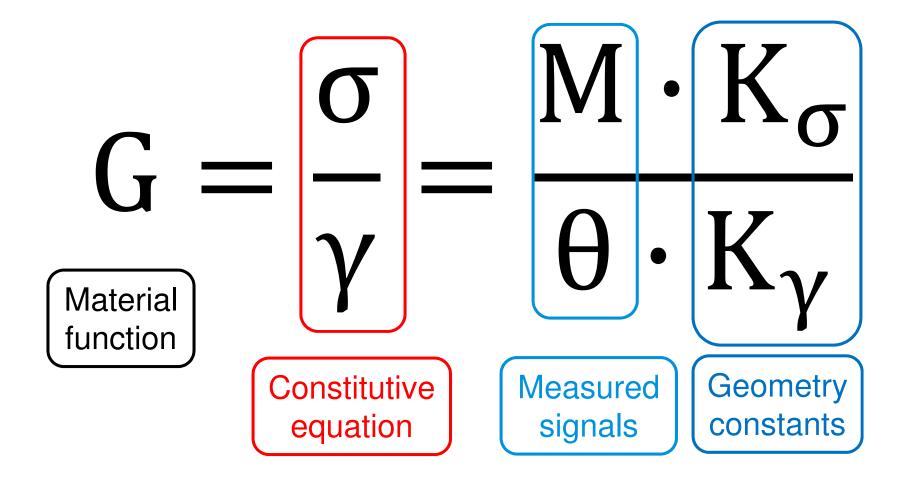
$\gamma = \theta \cdot K_\gamma$

• γ = shear strain (no units)

- $\bullet \theta$ = angular displacement (radians)
- • K_{γ} = strain constant
- The strain constant, K_{γ} , is dependent on measurement geometry and/or initial sample dimensions
- Calculate percent strain (γ %) by multiplying strain by 100



Equation for modulus





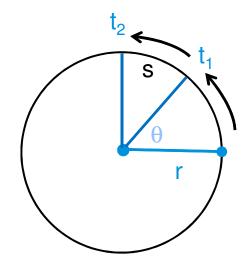
Measured parameter: angular velocity

Angular velocity (Ω) is the change in angular displacement
 (θ) per unit time of measurement

•Note: linear velocity $V = \Delta s / \Delta t$

 $\Omega = \Delta \theta / \Delta t$

Ω = angular velocity (radians/s)
θ = angular displacement (radians)
t = time (s)





Calculated parameter: shear rate

 Shear rate is calculated from the angular velocity and geometry strain constant

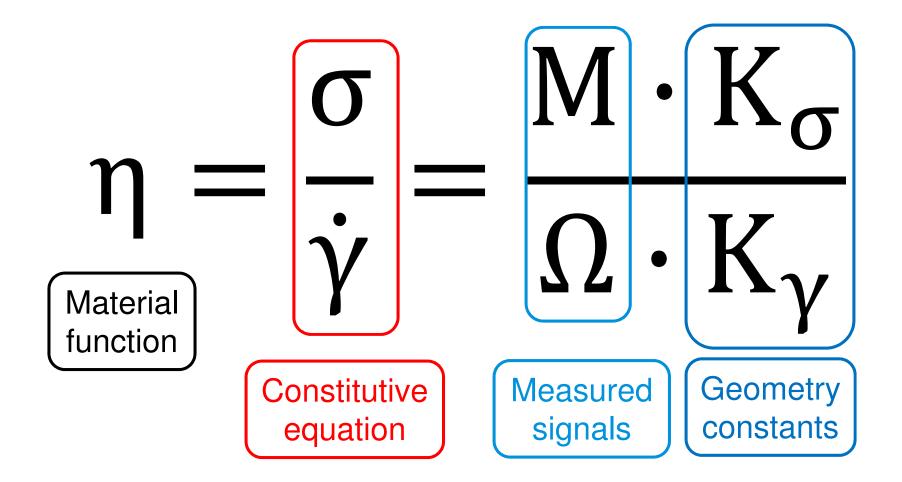
$$\dot{\gamma} = \Omega \cdot K_{\gamma}$$

•
$$\dot{\gamma}$$
 = shear rate (s⁻¹)
• Ω = angular velocity (radians/s)
• K_{γ} = strain constant

• The strain constant, K_{γ} , is dependent on measurement geometry and/or initial sample dimensions



Equation for viscosity





Five Important Rheometer Specifications

- Torque range
- Angular Resolution
- Angular Velocity Range
- Frequency Range
- Normal Force



Discovery Hybrid Rheometer Specifications

Specification	HR-3	HR-2	HR-1
Bearing Type, Thrust	Magnetic	Magnetic	Magnetic
Bearing Type, Radial	Porous Carbon	Porous Carbon	Porous Carbon
Motor Design	Drag Cup	Drag Cup	Drag Cup
Minimum Torque (nN.m) Oscillation	0.5	2	10
Minimum Torque (nN.m) Steady Shear	5	10	20
Maximum Torque (mN.m)	200	200	150
Torque Resolution (nN.m)	0.05	0.1	0.1
Minimum Frequency (Hz)	1.0E-07	1.0E-07	1.0E-07
Maximum Frequency (Hz)	100	100	100
Minimum Angular Velocity (rad/s)	0	0	0
Maximum Angular Velocity (rad/s)	300	300	300
Displacement Transducer	Optical encoder	Optical encoder	Optical encoder
Optical Encoder Dual Reader	Standard	N/A	N/A
Displacement Resolution (nrad)	2	10	10
Step Time, Strain (ms)	15	15	15
Step Time, Rate (ms)	5	5	5
Normal/Axial Force Transducer	FRT	FRT	FRT
Maximum Normal Force (N)	50	50	50
Normal Force Sensitivity (N)	0.005	0.005	0.01
Normal Force Resolution (mN)	0.5	0.5	1



DHR - DMA mode (optional)		
Motor Control	FRT	
Minimum Force (N) Oscillation	0.1	
Maximum Axial Force (N)	50	
Minimum Displacement (µm) Oscillation	1.0	
Maximum Displacement (µm) Oscillation	100	
Displacement Resolution (nm)	10	
Axial Frequency Range (Hz)	1 x 10 ⁻⁵ to 16	



ARES-G2 Rheometer Specifications

Force/Torque Rebalance Transducer (Sample Stress)		
Transducer Type	Force/Torque Rebalance	
Transducer Torque Motor	Brushless DC	
Transducer Normal/Axial Motor	Brushless DC	
Minimum Torque (µN.m) Oscillation	0.05	
Minimum Torque (µN.m) Steady Shear	0.1	
Maximum Torque (mN.m)	200	
Torque Resolution (nN.m)	1	
Transducer Normal/Axial Force Range (N)	0.001 to 20	
Transducer Bearing	Groove Compensated Air	

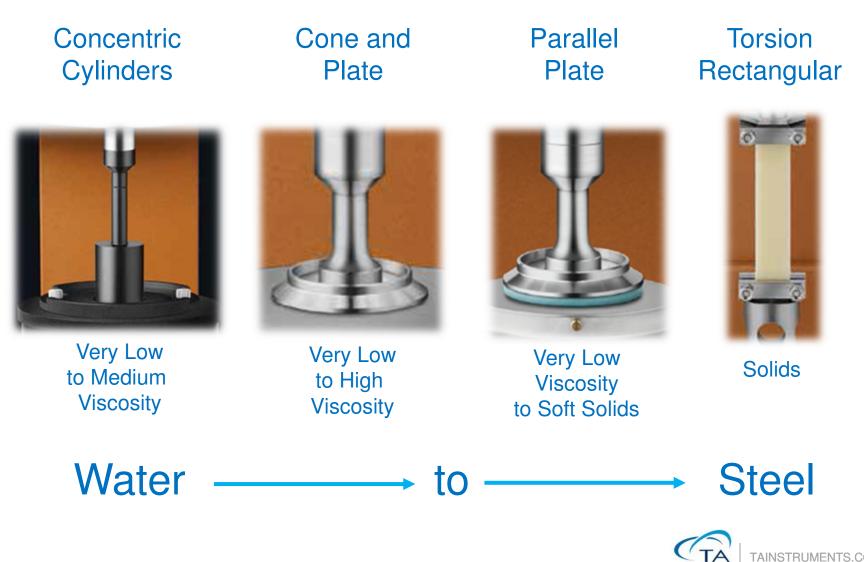
Driver Motor (Sample Deformation)		
Maximum Motor Torque (mN.m)	800	
Motor Design	Brushless DC	
Motor Bearing	Jeweled Air, Sapphire	
Displacement Control/ Sensing	Optical Encoder	
Strain Resolution (µrad)	0.04	
Minimum Angular Displacement (µrad)	1	
Oscillation		
Maximum Angular Displacement (µrad)	Unlimited	
Steady Shear		
Angular Velocity Range (rad/s)	1x 10 ⁻⁶ to 300	
Angular Frequency Range (rad/s)	1x 10 ⁻⁷ to 628	
Step Change, Velocity (ms)	5	
Step Change, Strain (ms)	10	



Orthogonal Superposition (OSP) and DMA modes		
Motor Control	FRT	
Minimum Transducer Force (N) Oscillation	0.001	
Maximum Transducer Force (N)	20	
Minimum Displacement (µm) Oscillation	0.5	
Maximum Displacement (µm) Oscillation	50	
Displacement Resolution (nm)	10	
Axial Frequency Range (Hz)	1 x 10 ⁻⁵ to 16	



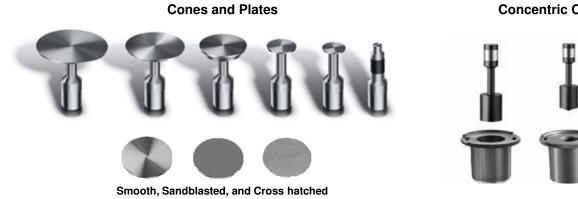
Geometry Options





Assess material to test

- · Geometry material of construction, size and surface
- In general, lower viscosity use larger diameter or larger contact area and higher viscosity or more solid-like smaller diameter
- Consider:
 - Volume requirements
 - Particle size, settling or mixing necessary
 - Loading procedure for structured substances (Pre-shear)
 - Evaporation seal sample edge, solvent trap, or RH accessory
 - Surface slip and edge fracture

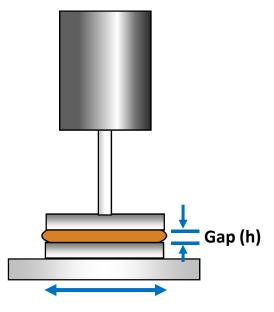


Concentric Cylinders (or Cups) and Rotors (or Bobs)





Parallel Plate



Diameter (2·r)

Strain Constant: $K_{\gamma} = \frac{r}{h}$

(to convert angular velocity, rad/sec, to shear rate, 1/sec, at the edge or angular displacement, radians, to shear strain (unitless) at the edge. The radius, r, and the gap, h, are expressed in meters)



(to convert torque, $N \cdot m$, to shear stress at the edge, Pa, for Newtonian fluids. The radius, r, is expressed in meters)



When to use Parallel Plates

- Low/Medium/High Viscosity Liquids
- Soft Solids/Gels
- Thermosetting materials
- Samples with large particles

- Samples with long relaxation time
- Temperature Ramps/ Sweeps
- Materials that may slip
 - Crosshatched or Sandblasted plates
- Small sample volume

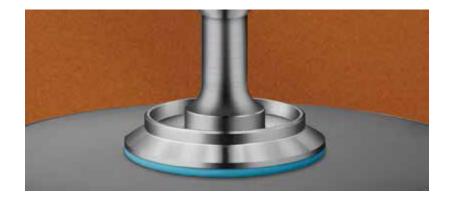
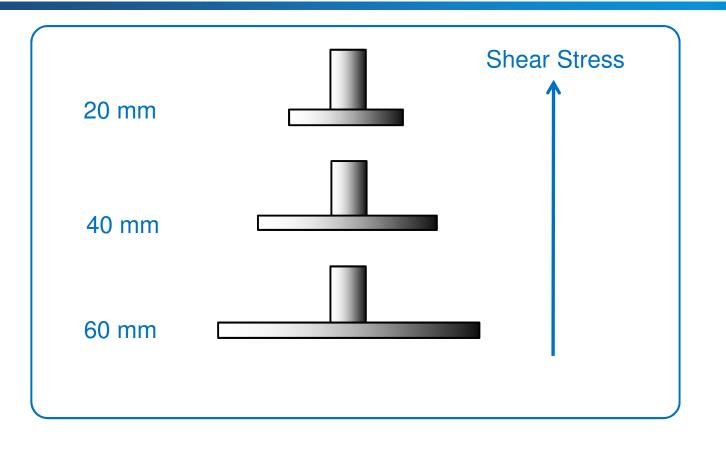




Plate Diameters

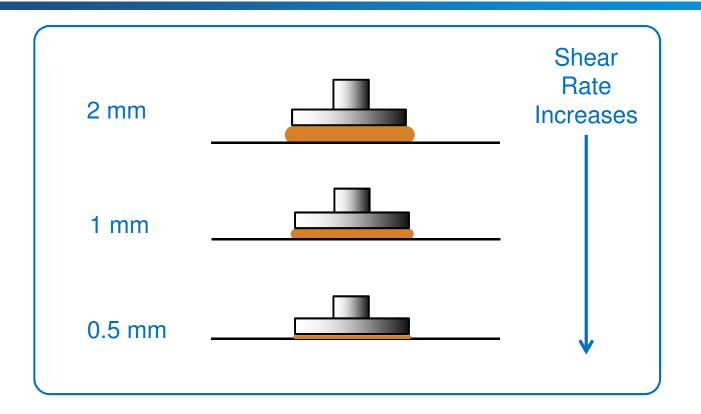


As diameter decreases, shear stress increases

$$\sigma = M \frac{2}{\pi r^3}$$



Plate Gaps



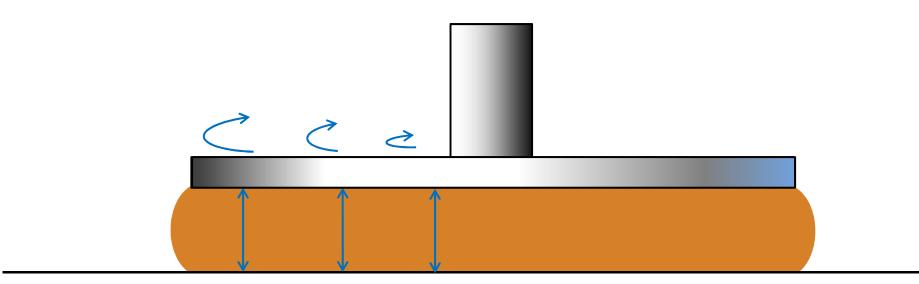
As gap height decreases, shear rate increases

 $\dot{\gamma} = \Omega \frac{r}{h}$



Effective Shear Rate varies across a Parallel Plate

 For a given angle of deformation, there is a greater arc of deformation at the edge of the plate than at the center



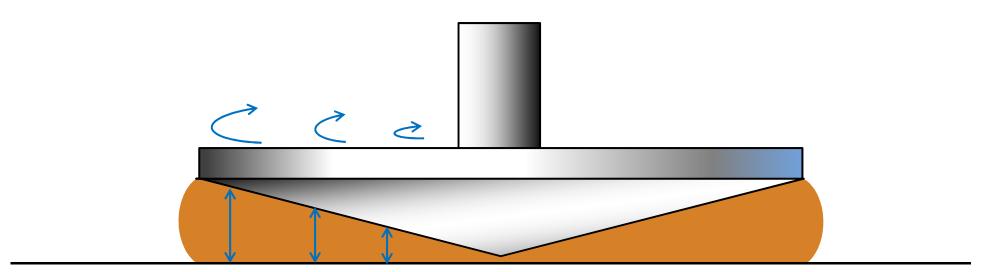
 $\gamma = \frac{dx}{h}$ dx increases further from the center, h stays constant

Single-point correction for the parallel plate geometry (0.76 radius) [M.S. Carvalho, M. Padmanabhan and C.W. Macosko, *J. Rheol.* 38 (1994) 1925-1936]



Shear Rate is Normalized across a Cone

 The cone shape produces a smaller gap height closer to inside, so the shear on the sample is constant



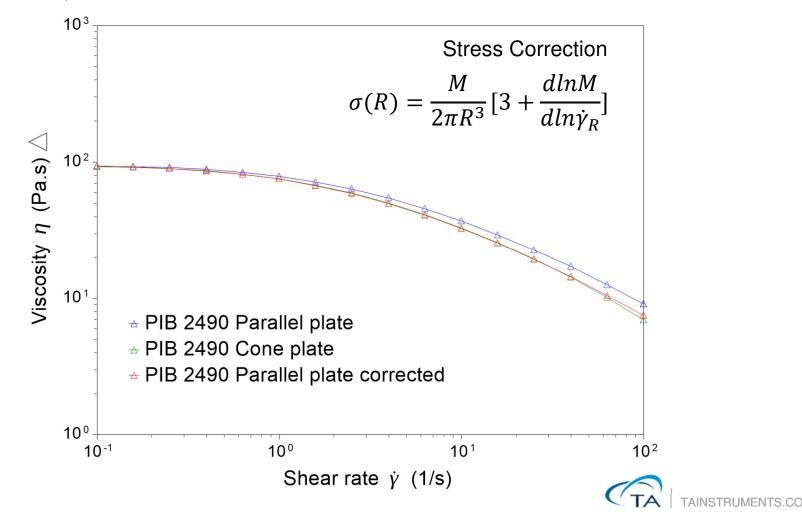
$$\gamma = \frac{dx}{h}$$

h increases proportionally to dx, γ is uniform

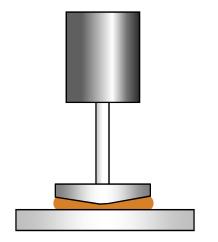


Parallel Plate Stress Correction

 The parallel plate viscosity can be corrected through the Weissenberg-Rabinowitsch correction so that parallel plate data can be compared with cone and plate data.



Cone and Plate

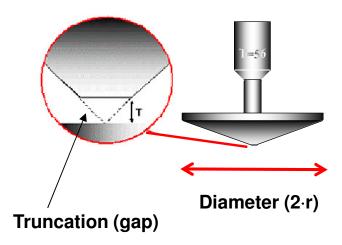


Strain Constant: $K_{\gamma} = \frac{1}{\beta}$

(to convert angular velocity, rad/sec, to shear rate. 1/sec, or angular displacement, radians, to shear strain, which is unit less. The angle, β , is expressed in radians)

Stress Constant:
$$K_{\sigma} = \frac{3}{2\pi r^3}$$

(to convert torque, $N \cdot m$, to shear stress, Pa. The radius, r, is expressed in meters)





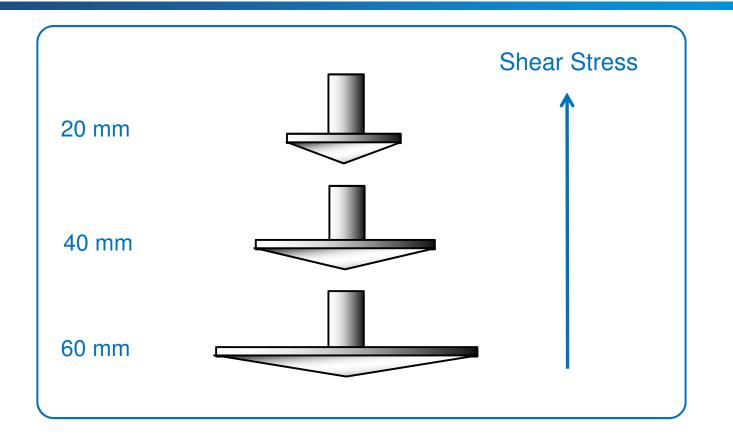
When to use Cone and Plate

- Very Low to High Viscosity Liquids
- High Shear Rate measurements
- Normal Stress Growth
- Unfilled Samples
- Isothermal Tests
- Small Sample Volume





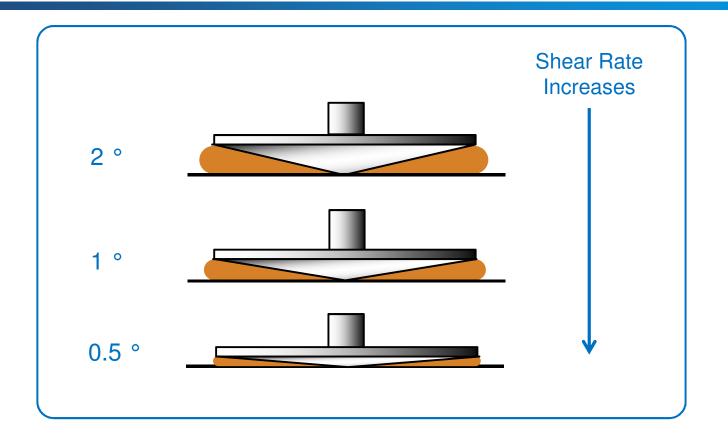
Cone Diameters



As diameter decreases, shear stress increases $\sigma = M \frac{3}{2\pi r^3}$



Cone Angles

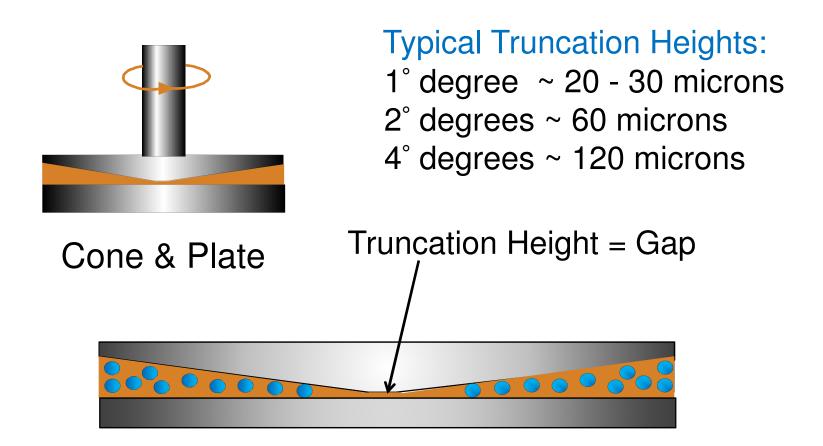


As cone angle decreases, shear rate increases

 $\dot{\gamma} = \Omega \frac{1}{\beta}$



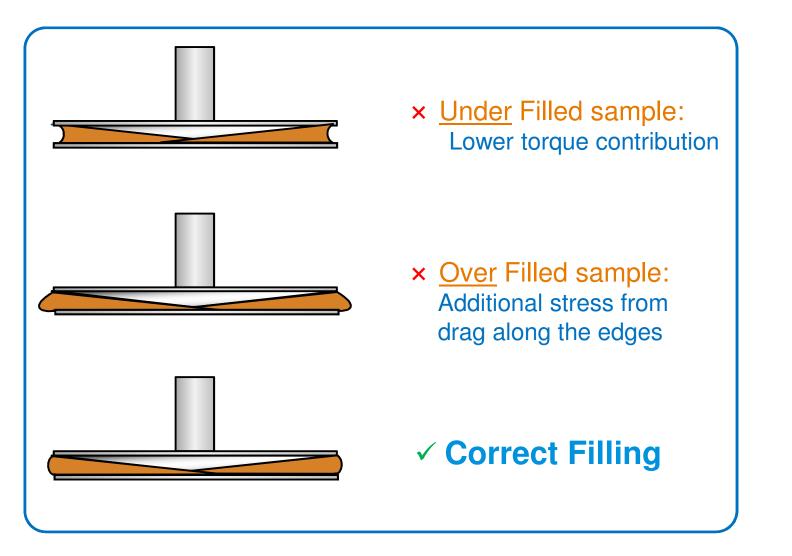
Limitations of Cone and Plate



Gap must be > or = 10 [particle size]!!

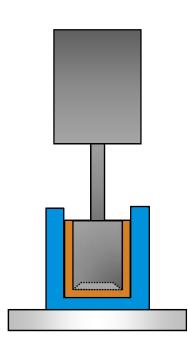


Correct Sample Loading – parallel plate and cone-plate

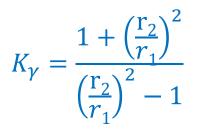




Concentric Cylinder



Strain Constant:



(to convert angular velocity, rad/sec, to shear rate, 1/sec, or angular displacement, radians, to shear strain (unit less). The radii, r_1 (inner) and r_2 (outer), are expressed in meters)

Stress Constant:

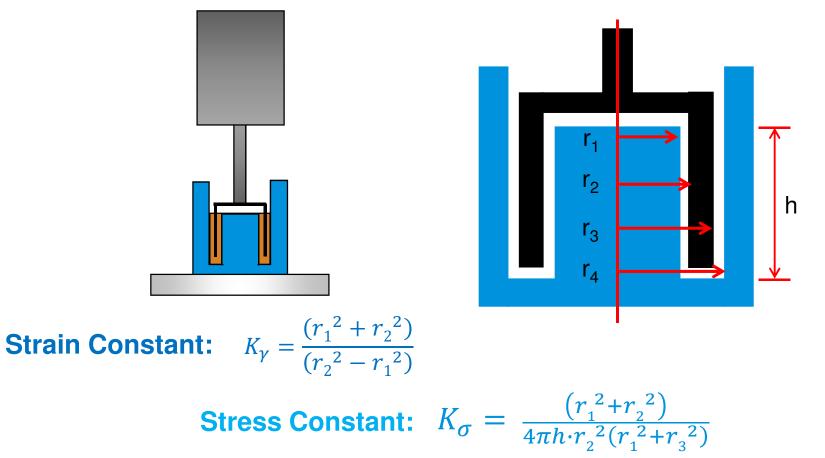
$$K_{\sigma} = \frac{1}{4\pi l} \left[\frac{1 + \left(\frac{r_2}{r_1}\right)^2}{c_l r_2^2} \right]$$

(to convert torque, N·m, to shear stress, Pa. The bob length, I, and the radius, r, are expressed in meters) c_{I} is the face factor



Double Wall

Use for very low viscosity systems (<1 mPas)





When to Use Concentric Cylinders



Peltier Concentric Cylinder



Electrically Heated Cylinder (EHC)

- Low to Medium Viscosity Liquids
- Unstable Dispersions and Slurries
- Minimize Effects of Evaporation
- Weakly Structured Samples (Vane)
- High Shear Rates



Peltier Concentric Cylinders



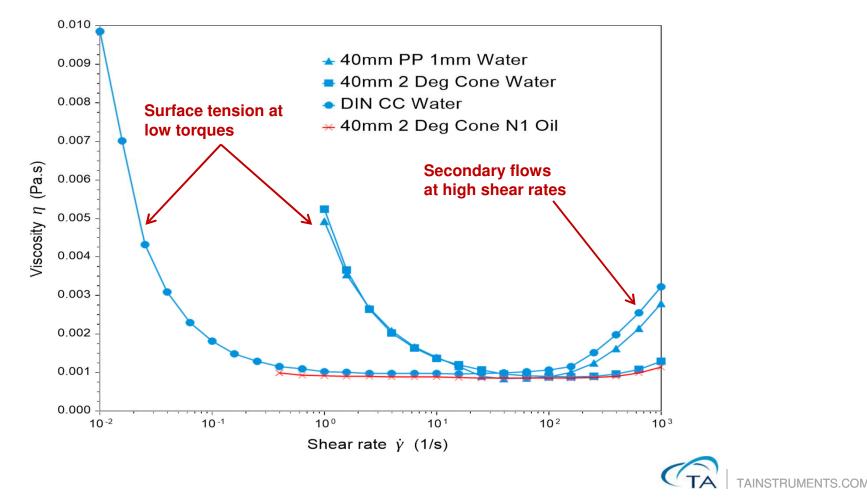
Concentric Cylinder Cup and Rotor Compatibility Chart

Cup/Rotor	DIN	Recessed End	Starch Impeller	Vane	Wide Gap Vane	Double Gap	Helical Rotor
Standard (rad= 15 mm)	•	•		•	•		
Large Diameter (rad= 22 mm)				•	•		•
Starch (rad= 18.5 mm)	•	•	•	•	•		•
Grooved				•	•		
Double Gap						•	
Helical (rad= 17 mm)							•

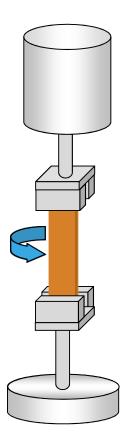


Viscosity of Water

- Surface tension causes artifact shear thinning under low torque
- Secondary flow shows artifact shear thickening under high shear
- Use a large diameter geometry with a smaller gap



Torsion Rectangular



$$K_{\gamma} = \frac{t}{l \left[1 - 0.378 \left(\frac{t}{w}\right)^2\right]}$$

$$K_{\tau} = \frac{\left(3 + \frac{1.8}{w}\right)}{\left(w \cdot t^2\right)}$$

Advantages:

- High modulus samples
- Small temperature gradient
- Simple to prepare

w = Width I = Length t = Thickness

Disadvantages:

 No pure Torsion mode for high strains

Torsion cylindrical also available



Torsion and DMA Measurements



- Torsion and DMA geometries allow solid samples to be characterized in a temperature controlled environment
 - Torsion measures G', G", and Tan δ
 - DMA measures E', E", and Tan δ
 - ARES G2 DMA is standard function (50 μm amplitude)
 - DMA is an optional DHR function (100 μm amplitude)



Rectangular and cylindrical torsion



DMA 3-point bending and tension (cantilever not shown)



Geometry Overview

Geometry	Application	Advantage	Disadvantage
Cone/plate	fluids, melts viscosity > 10mPas	true viscosities	temperature ramp difficult
Parallel Plate	fluids, melts viscosity > 10mPas	easy handling, temperature ramp	shear gradient across sample
Couette	low viscosity samples < 10 mPas	high shear rate	large sample volume
Double Wall Couette	very low viscosity samples < 1mPas	high shear rate	cleaning difficult
Torsion Rectangular	solid polymers, composites	glassy to rubbery state	Limited by sample stiffness
DMA	Solid polymers, films, Composites	Glassy to rubbery state	Limited by sample stiffness (Oscillation and stress/strain)



Setting up Rheological Experiments Flow Tests



Newtonian & Non-Newtonian Behavior

Newtonian

- Viscosity independent from shear rate and shear stress
- Viscosity only changes with temperature

Non- Newtonian

- Viscosity is shear dependent
 - Decrease with shear shear thinning
 - Increase with shear shear thickening
- Viscosity is time dependent
 - ✓ Decrease with time Thixotropic
 - Increase with time Rheopectic



Viscosity Values

Materials	Viscosity η (Pa.s)
Air /Gas	0.00001
Water	0.001
Milk/ Coffee	0.01
Olive oil	0.1
Glycerol	1
Liquid Honey	10
Molasses	100
Polymer Melt	1000
Asphalt Binder	100,000











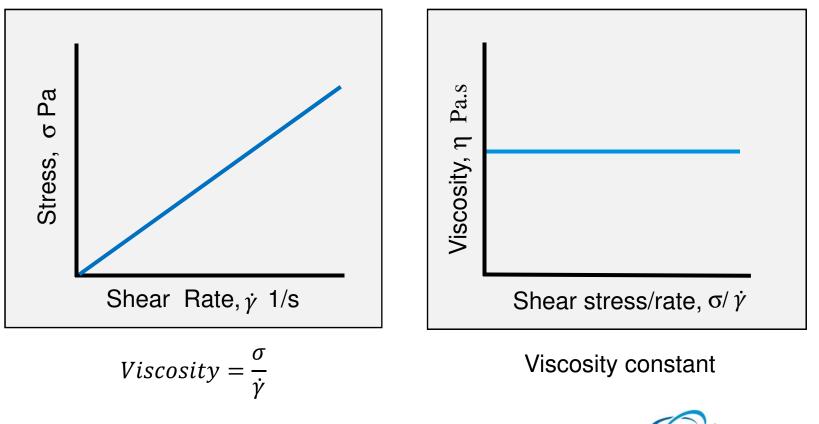




Newtonian Fluids

- Viscosity independent of shear rate and shear stress
- Examples:

water, acetone, ethanol, glycol, glycerin, cooking oil etc.

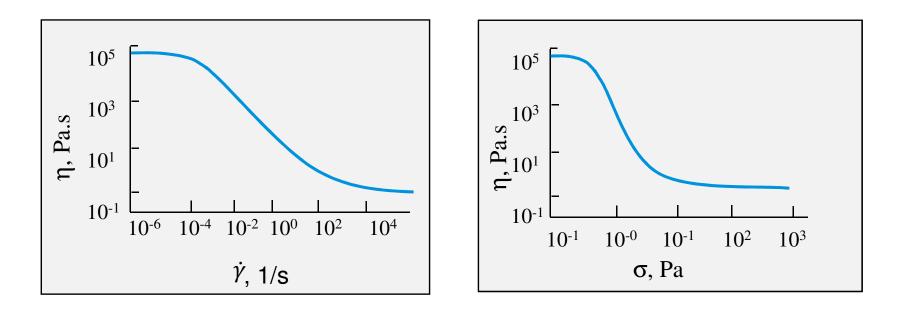




Shear Thinning Fluids

- Viscosity decrease with shear rate and shear stress
- Examples:

hand wash, paint, coating, shampoo....

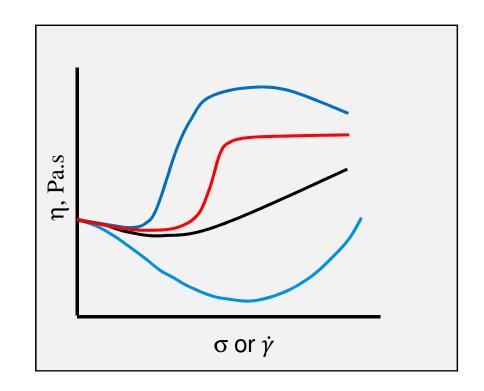




Shear Thickening Fluids

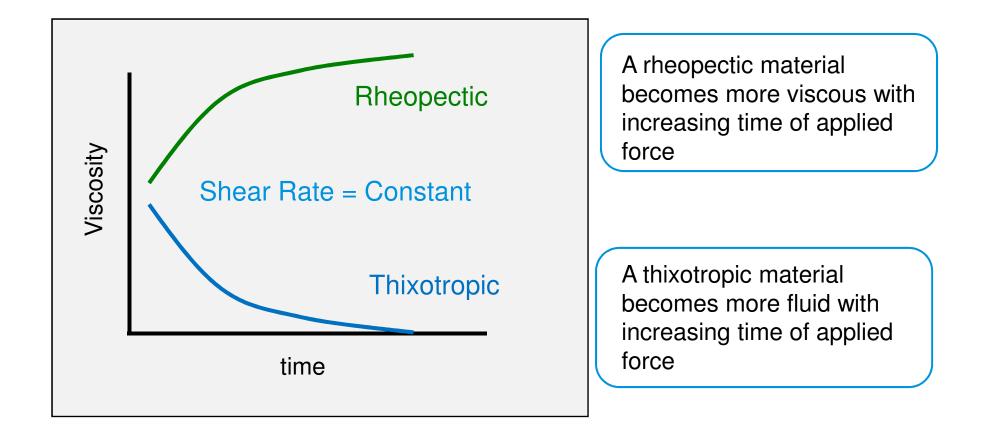
- Viscosity increase with shear rate and shear stress
- Examples:

highly concentrated cornstarch slurry; mud slurry



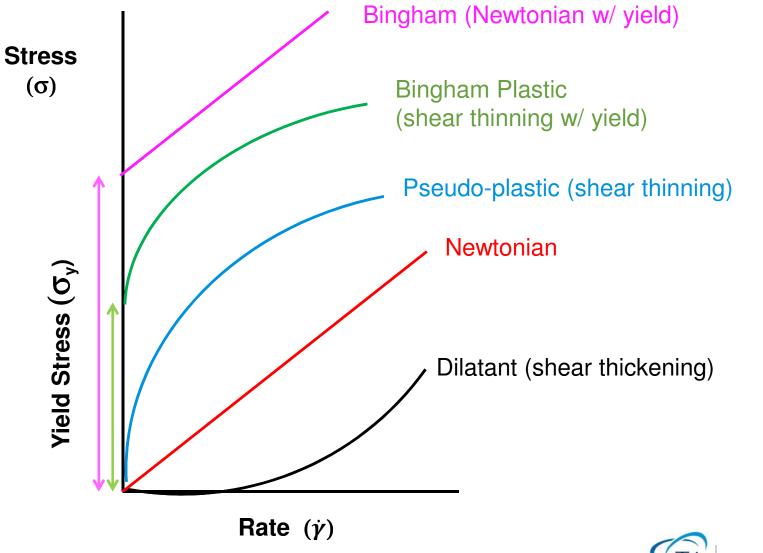


Time Dependent Fluids





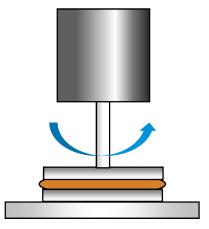
Summary of Flow Diagrams

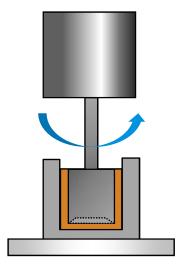


Rheological Methods

 Common rheological methods for measuring viscosity of liquids

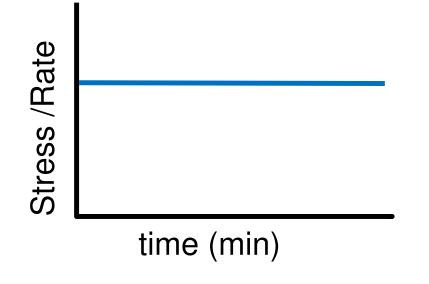
Single rate/stress flow
Continuous rate/stress ramp
Stepped or steady state flow
Flow temperature ramp







Single Rate/Stress Test



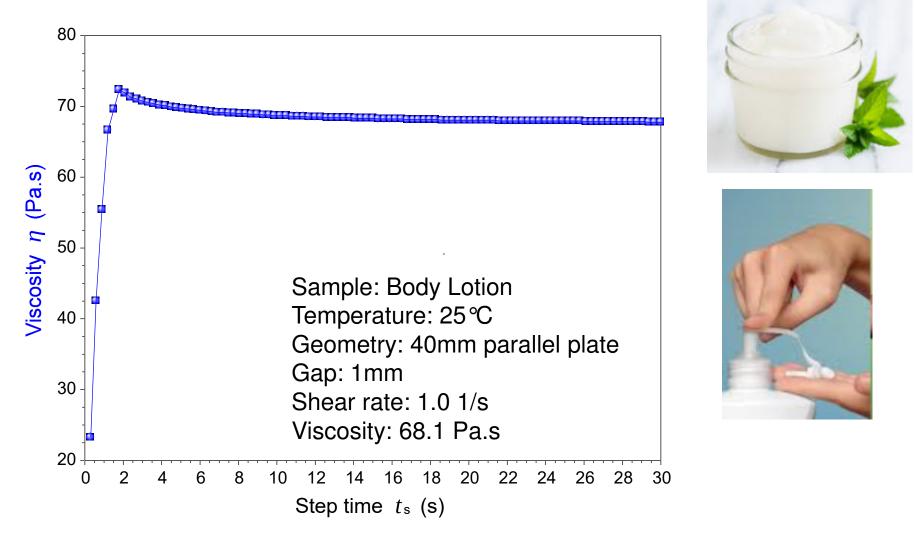
- Isothermal temperature
- Constant rate vs. time
- Constant stress vs. time

<u>USES</u>

- Single point testing
- Scope the time for steady state under certain rate

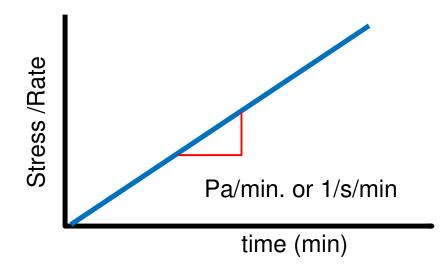


Body Lotion: Single Rate Test





Continuous Ramp



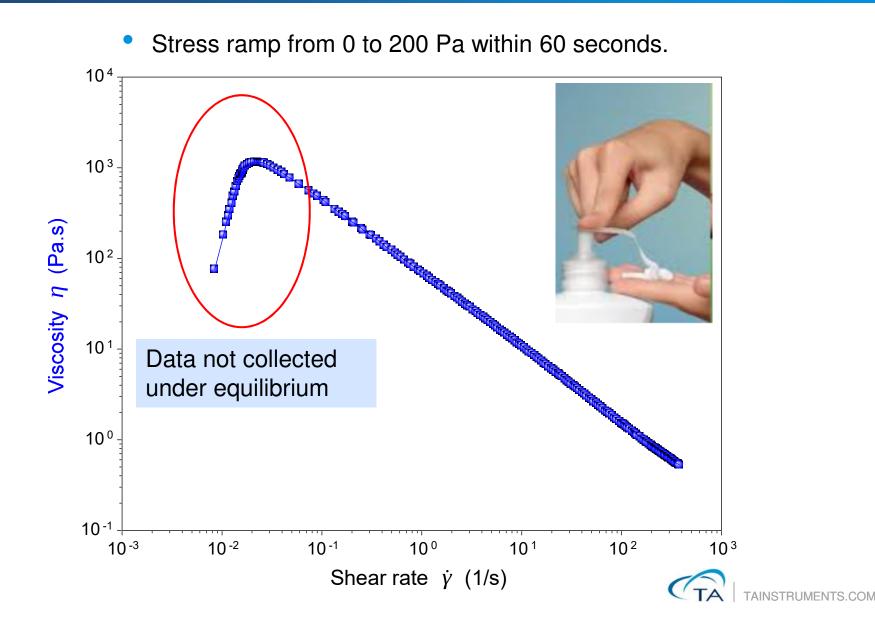
- Isothermal temperature
- Ramp stress or shear rate at a constant speed

<u>USES</u>

- Scouting viscosity over wide range of shear
- Measure yield stress

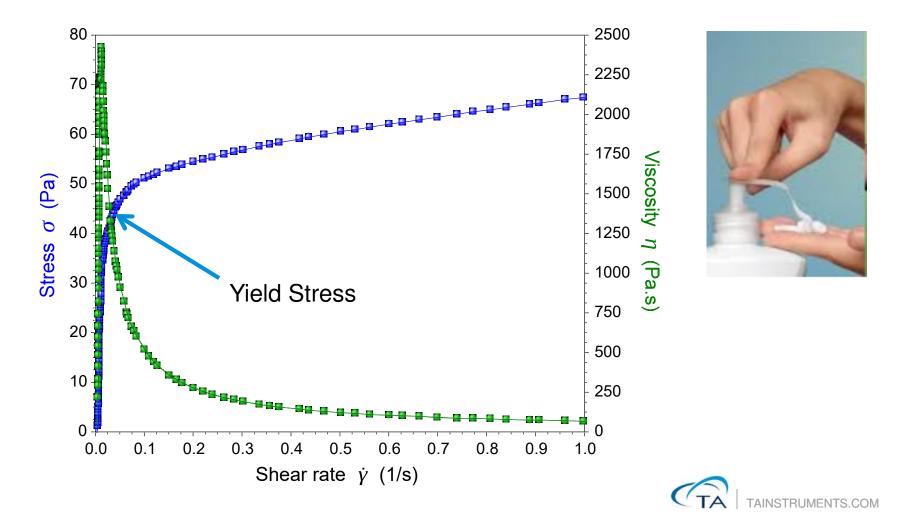


Viscosity of a Body Lotion

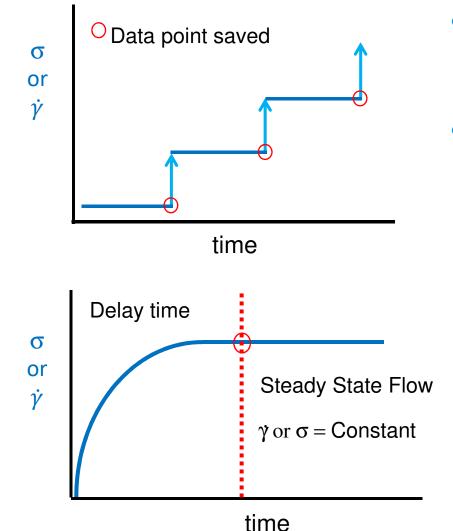


Measure Yield Stress of a Body Lotion

 Body lotion does not flow unless the applied stress exceeds a certain value – the yield point.



Stepped or Steady-State Flow



- Step stress or shear rate from low to high on a logarithmic scale
- At each step, viscosity is measured when steady state has been reached

Viscosity Flow Curves

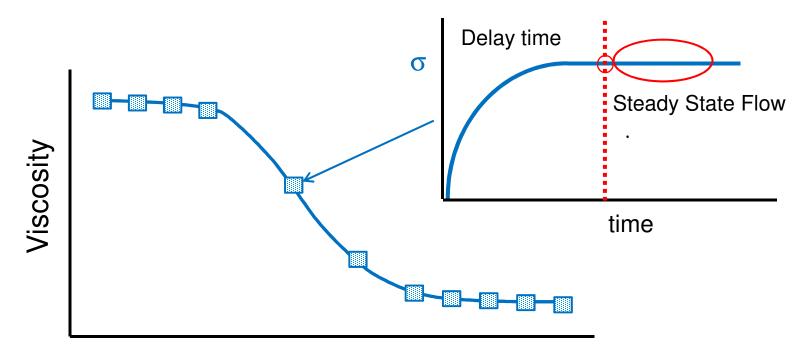
USES

Yield Stress Measurements



Stepped or Steady-State Flow

- At each point, viscosity is measured at steady state
- Provides the most precise shear viscosity versus shear rate determination



Shear Rate, 1/s



DHR and ARES G2: Steady State Algorithm

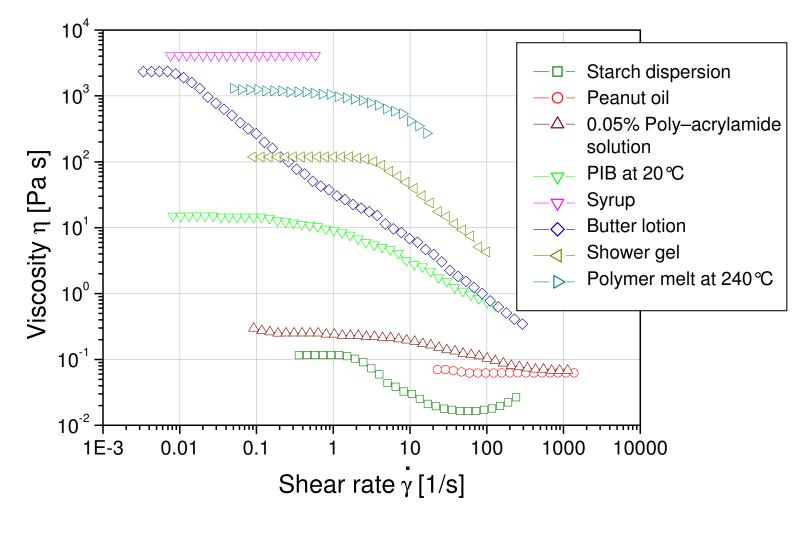
2: Flow Sweep

Environmental Control				
Temperature	25	°C	Inherit Set Point	
Soak Time	01:00	hh:mm:ss	📝 Wait For Temperature	Control variable
Test Parameters				Shear rate
Logarithmic sweep			•	 Velocity
Shear rate	0.1	to 100.0	1/s 🗸	Torque
Points per decade	5			 Shear stress
Steady state sensi			1	
Max. equilibration time	-	hh:mm:ss	,	
	10	hh:mm:ss		
Sample period		nn.mm:ss		Steady state alg
% tolerance	5.0			
Consecutive within	3			
Scaled time average	ge			

Controlled Rate Advanced



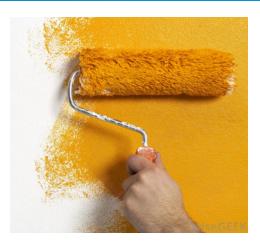
Viscosity Curves of Various Fluids





Typical Applications Shear Rates

Process	Shear Rate (1/s)
sedimentation	10 ⁻⁵ – 10 ⁻²
leveling and sagging	10 ⁻² – 1
chewing, swallowing, dipping coating,	1 – 10 ²
pipe flow, pumping, mixing, stirring	1 – 10 ³
brushing, painting, extruding	$10^2 - 10^4$
milling, spraying, rubbing	$10^3 - 10^5$
high speed coating	>10 ⁵



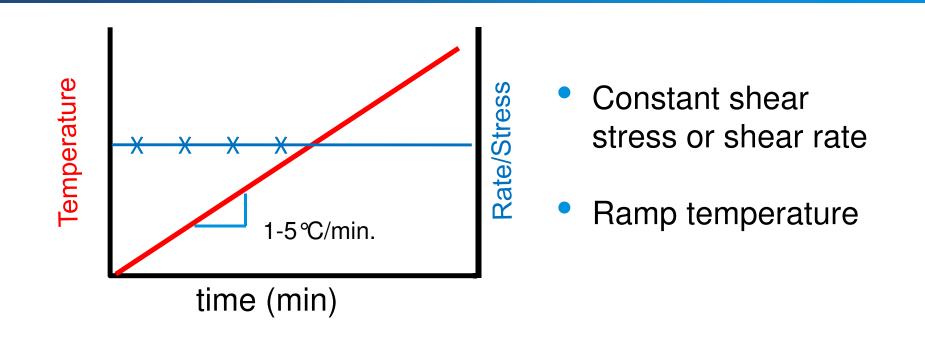








Flow Temperature Ramp

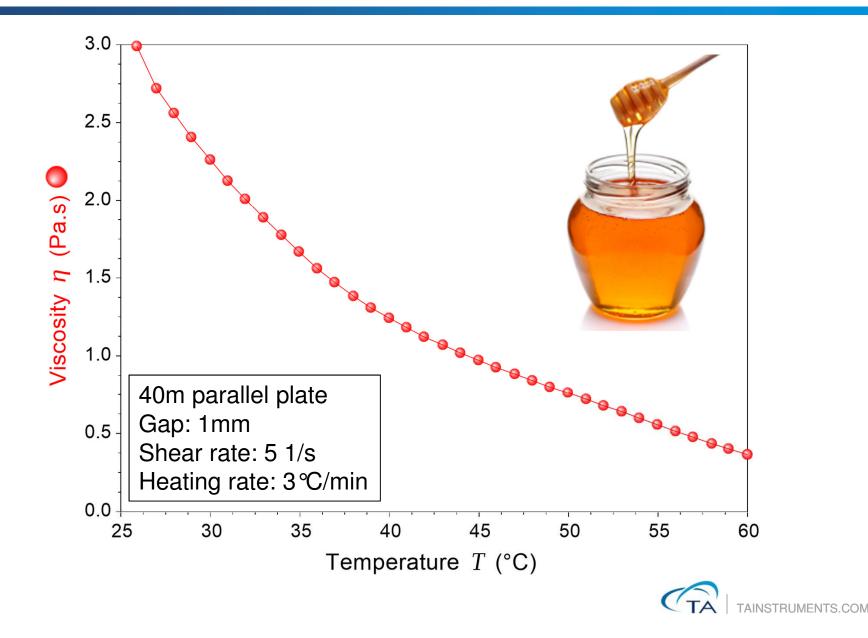


<u>USES</u>

• Measure the viscosity change vs. temperature



Viscosity of Honey: Temperature Dependence



Setting up Rheological Experiments Oscillatory Tests



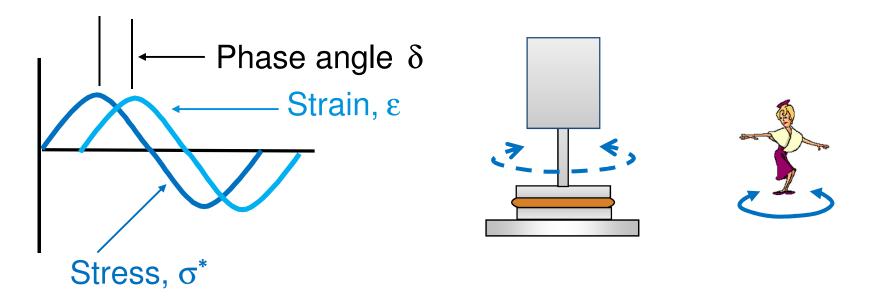
Outline

- Understanding Oscillation
- Approach to Oscillation Experimentation
 - Stress and Strain Sweep
 - Time Sweep
 - Frequency Sweep
 - Temperature Ramp
 - Temperature Sweep (TTS)



Dynamic Oscillatory Tests

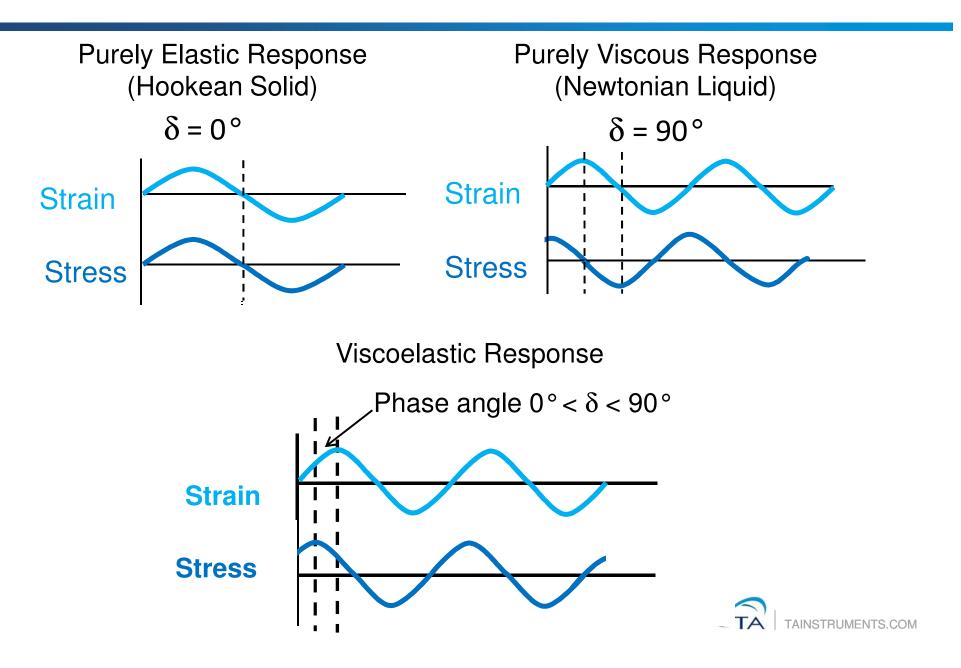
Most commonly used tests in adhesive evaluations



- Apply a sinusoidal stress to the sample at a certain frequency
- Monitor sample response in strain deformation
- The shift between the input stress and output strain is the phase angle



Dynamic Testing: Response for Classical Extremes



Viscoelastic Parameters

<u>The Modulus:</u> Measure of materials overall resistance to deformation.

<u>The Elastic (Storage) Modulus:</u> Measure of elasticity of material. The ability of the material to store energy.

<u>The Viscous (loss) Modulus:</u> The ability of the material to dissipate energy. Energy lost as heat.

<u>Tan Delta:</u>

Measure of material damping such as vibration or sound damping.

$$G^* = \left(\frac{\text{Stress}^*}{\text{Strain}}\right)$$

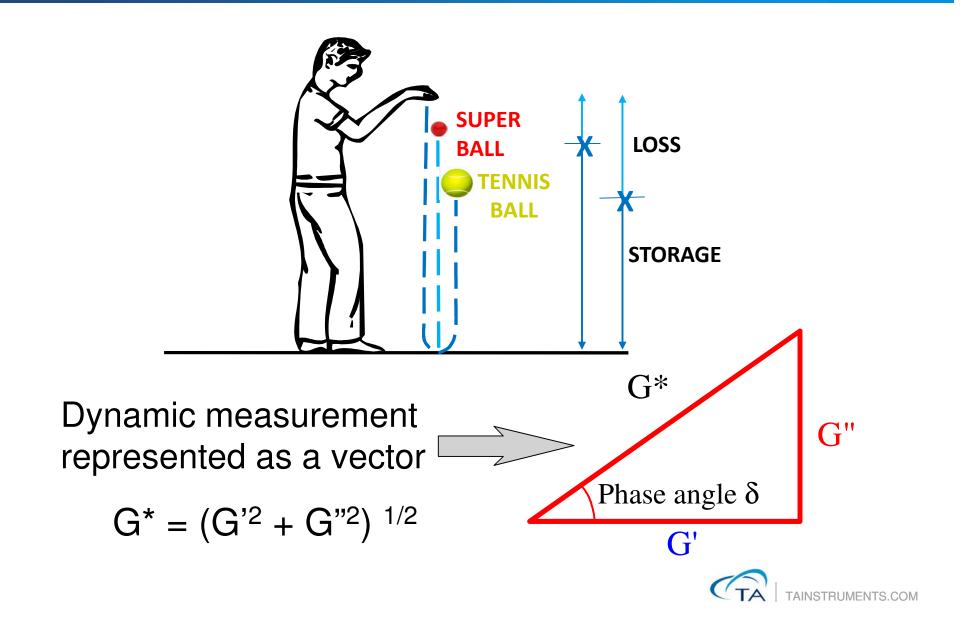
$$G' = \left(\frac{\text{Stress}^*}{\text{Strain}}\right)\cos\delta$$

$$G'' = \left(\frac{Stress^*}{Strain}\right) \sin \delta$$

$$\tan \delta = \left(\frac{G'}{G'}\right)$$



Storage and Loss of a Viscoelastic Material



Complex Viscosity

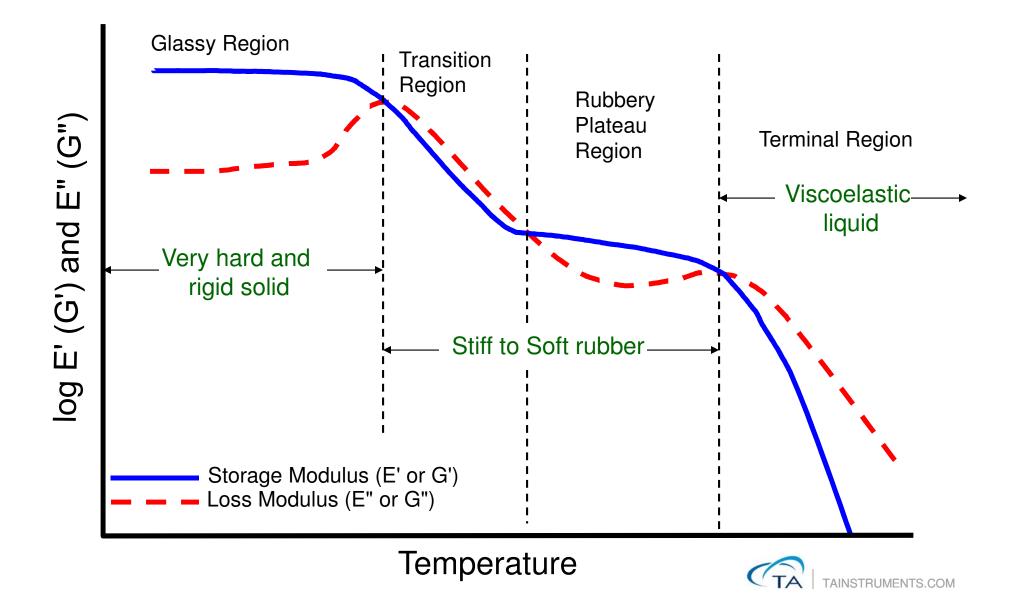
- The viscosity measured in an oscillatory experiment is a Complex Viscosity much the way the modulus can be expressed as the complex modulus. The complex viscosity contains an elastic component and a term similar to the steady state viscosity.
 - The Complex viscosity is defined as:

```
\eta^* = \eta' - i \eta''
or
\eta^* = G^*/\omega
```

Note: frequency must be in rad/sec!



Viscoelastic Spectrum for a Typical Amorphous Polymer

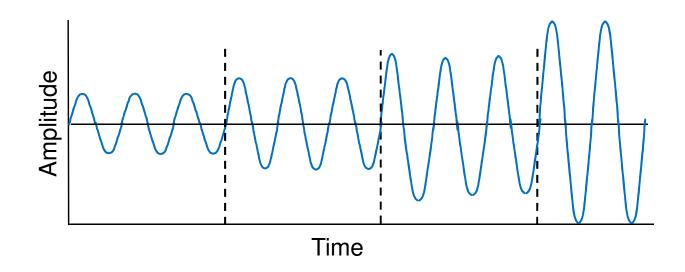


Dynamic oscillation methods

- •Stress, strain, or amplitude sweep
- Time sweep
- Frequency sweep
- Temperature ramp
- •Temperature sweep (or step)
 - Time temperature superposition (TTS)



Strain, stress, or amplitude sweep

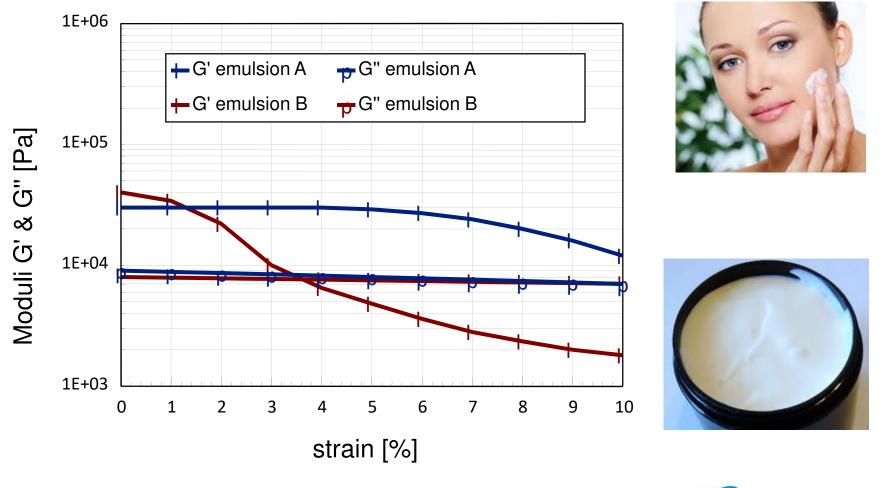


- The material response to increasing deformation amplitude is monitored at a constant frequency and temperature
- Determine LVR or yield stress
 - Tests assumes sample is stable



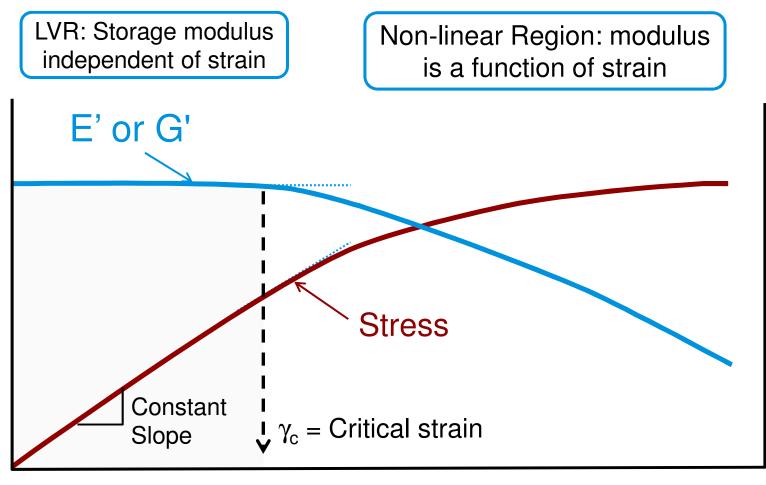
Creams/Lotions: Predict Stability

Stability, phase separation of a cosmetic cream





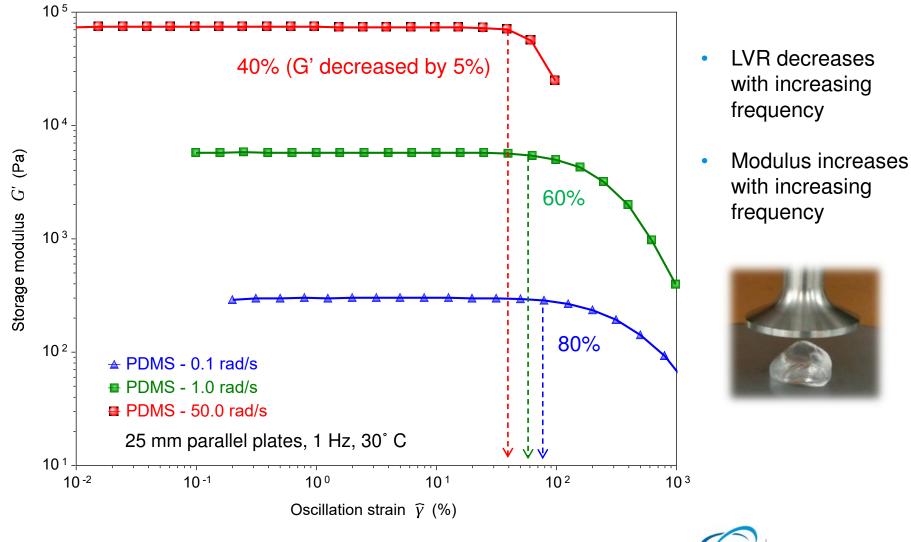
Dynamic Strain Sweep: Material Response



Strain (amplitude)



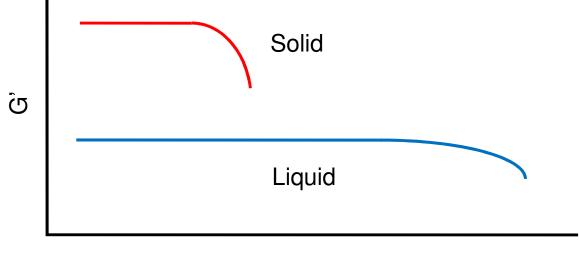
Frequency dependence of LVR





Temperature Dependence of LVR

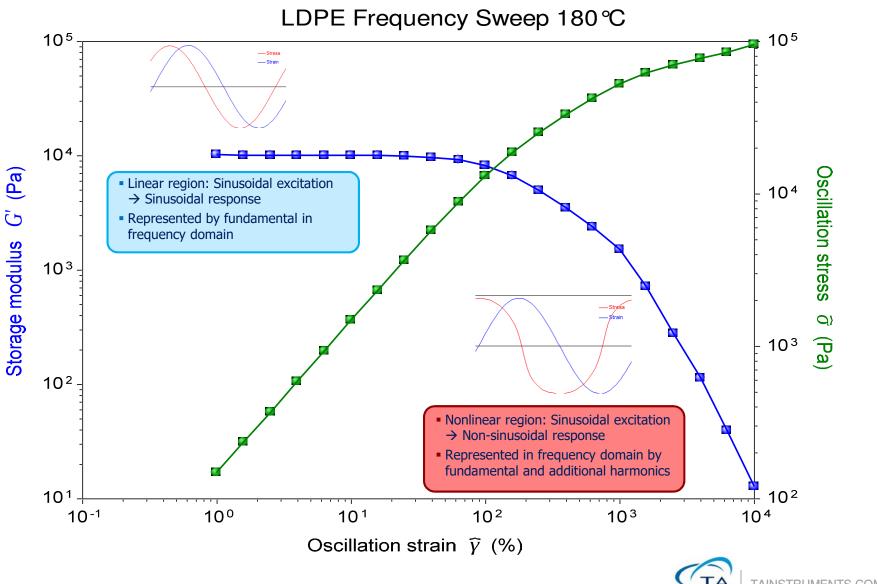
 In general, the LVR is shortest when the sample is in its most solid form.



% strain

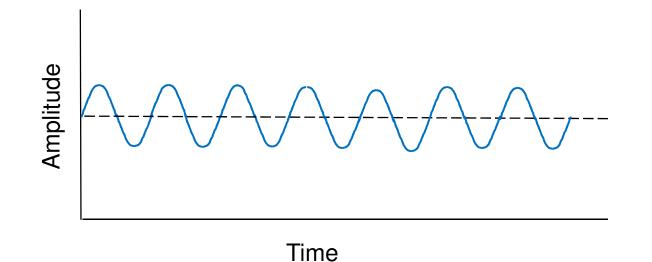


Linear and Non-linear Viscoelasticity



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Time sweep



- The material response is monitored at a constant frequency, amplitude, and temperature
- Determine stability (e.g. evaporation, degradation), thixotropy, and curing studies
 - Amplitude within LVR



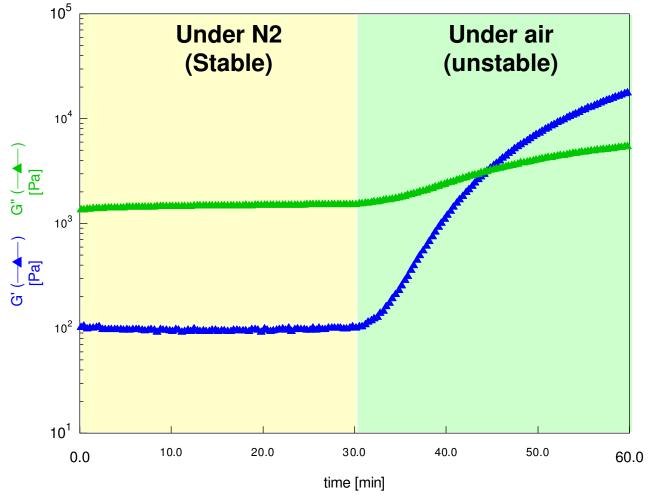
Importance of Time Sweep

- Important, but often overlooked
- Determines if properties are changing over the time of testing
 - Complex Fluids or Dispersions
 - Drying or volatilization (use solvent trap)
 - Structure recovery
 - Thixotropy
 - Polymers
 - Degradation (inert purge)
 - Curing



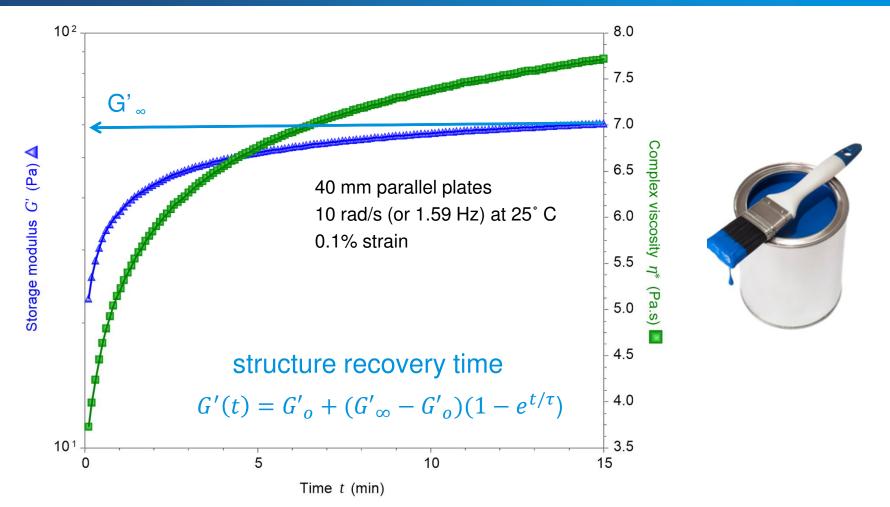
Time Sweep on PEEK Melt - Thermal Stability

2000G time sweep at 400 ℃





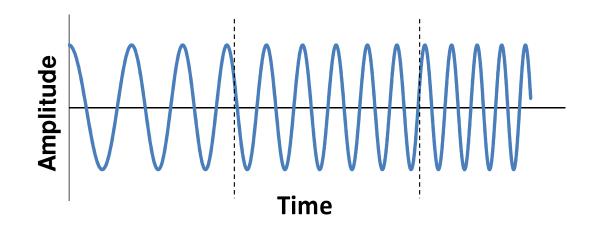
Structure Recovery of a Paint



- Monitor the increase of the G' or complex viscosity as function of time
- Thixotropic recovery can be described by the recovery time (τ)
 - Rule out evaporation







- The material response to increasing frequency (rate of deformation) is monitored at a constant amplitude and temperature
- Determine stability over the expected duration of test
 - Low frequencies = longer times
 - Amplitude within LVR



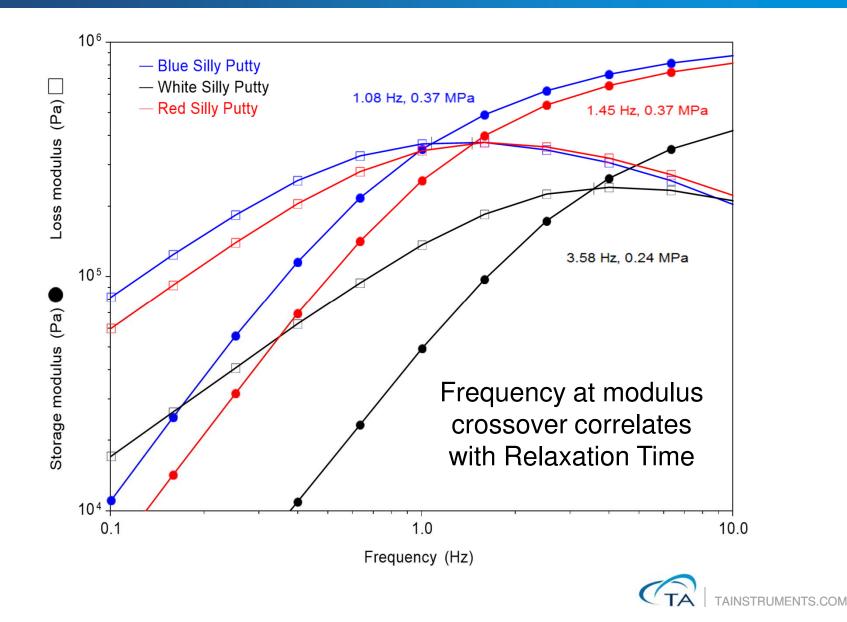
Time-Dependent Viscoelastic Behavior



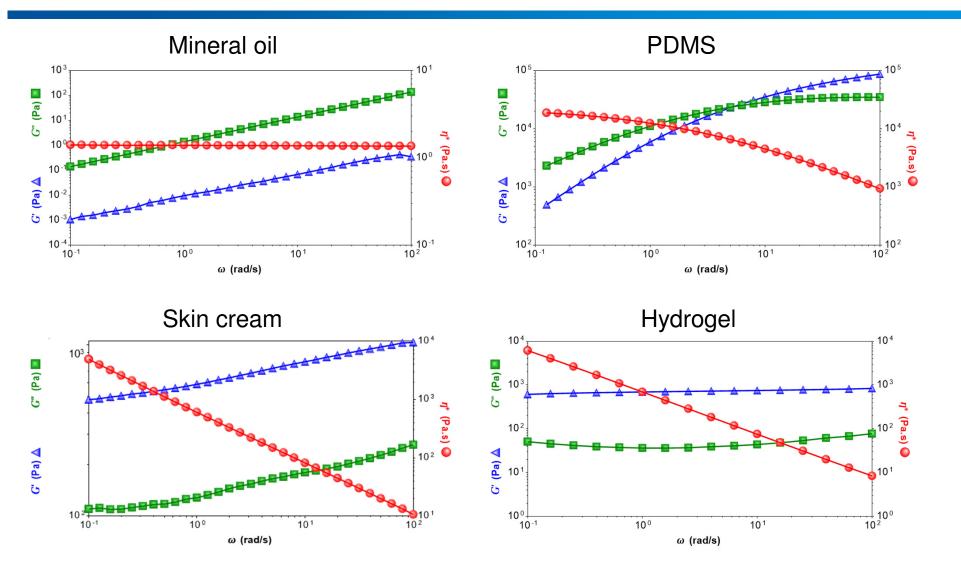
- Silly Putties have different characteristic relaxation times
- Dynamic (oscillatory) testing can measure time-dependent viscoelastic properties more efficiently by varying frequency (deformation time)



Frequency Sweep- Time Dependent Viscoelastic Properties

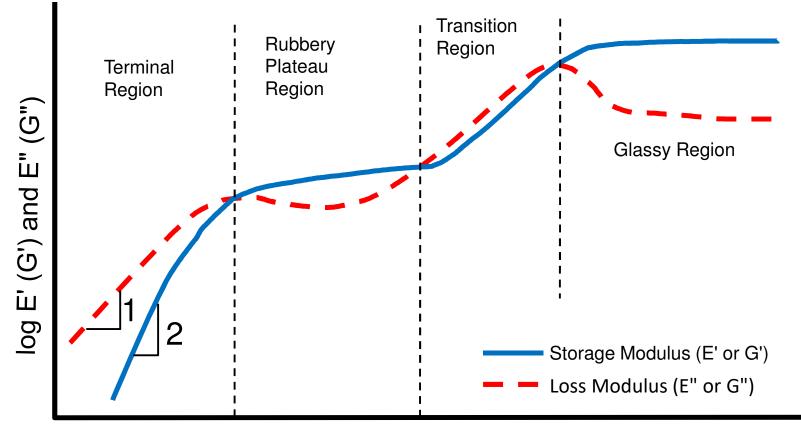


Differences in elasticity using frequency sweep





Frequency Sweep: Material Response



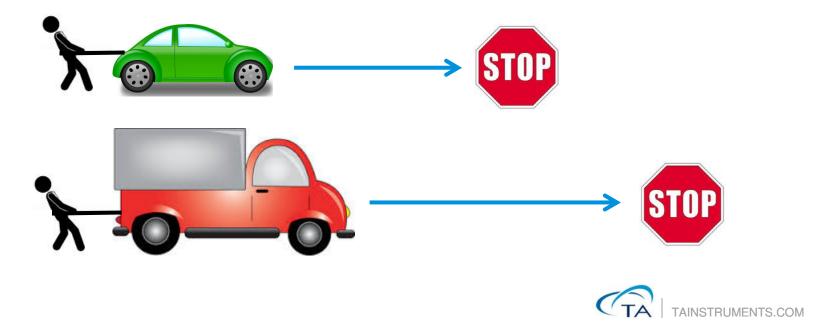
log Frequency (rad/s or Hz)



Inertial Effects

What is Inertia?

- <u>Definition</u>: That property of matter which manifests itself as a resistance to any change in momentum of a body
- Instrument has inertia
- Sample has inertia



Inertial Effects in Oscillation for DHR

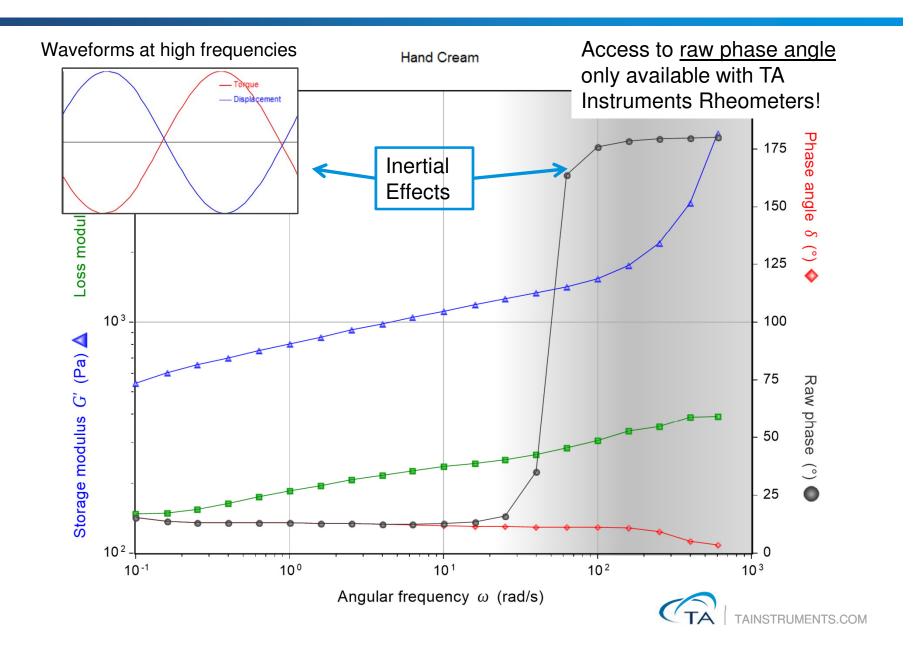
Inertia consideration

- Viscosity limitations with frequency
- Minimize inertia by using low mass geometries
- Monitor inertia using Raw Phase in degree
- When Raw Phase is greater than:
 - 150° degrees for AR series
 - 175° degrees for DHR series
 - This indicates that the system inertia is dominating the measurement signal. Data may not be valid

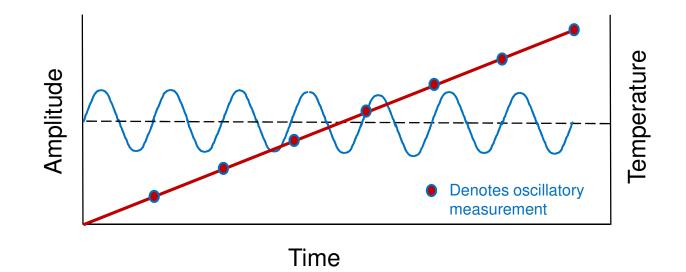
Raw Phase × Inertia Correction = delta



DHR Correction for Inertia



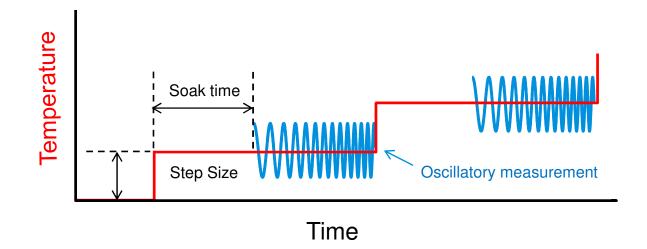
Dynamic temperature ramp



- Linear heating rate is applied and the material response is monitored at a constant frequency and constant amplitude
- Common heating/cooling rate: 2-5 °C/min
- Amplitude within LVR



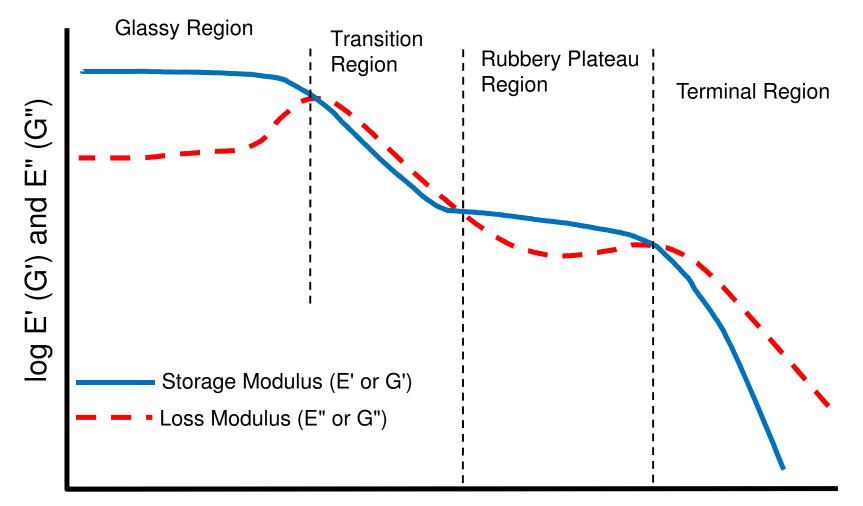
Temperature sweep (or step) - Single /Multi-Frequency



- Step and hold temperature then monitor material response
 - No thermal lag
- Common step: 5-10 degrees per step
- Amplitude within LVR



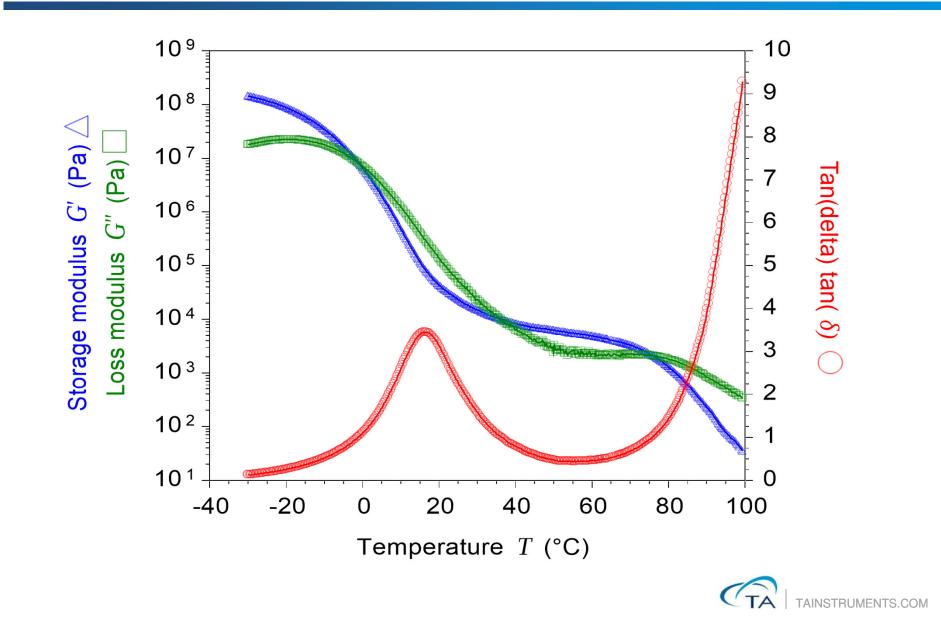
Dynamic Temperature Ramp or Sweep: Material Response



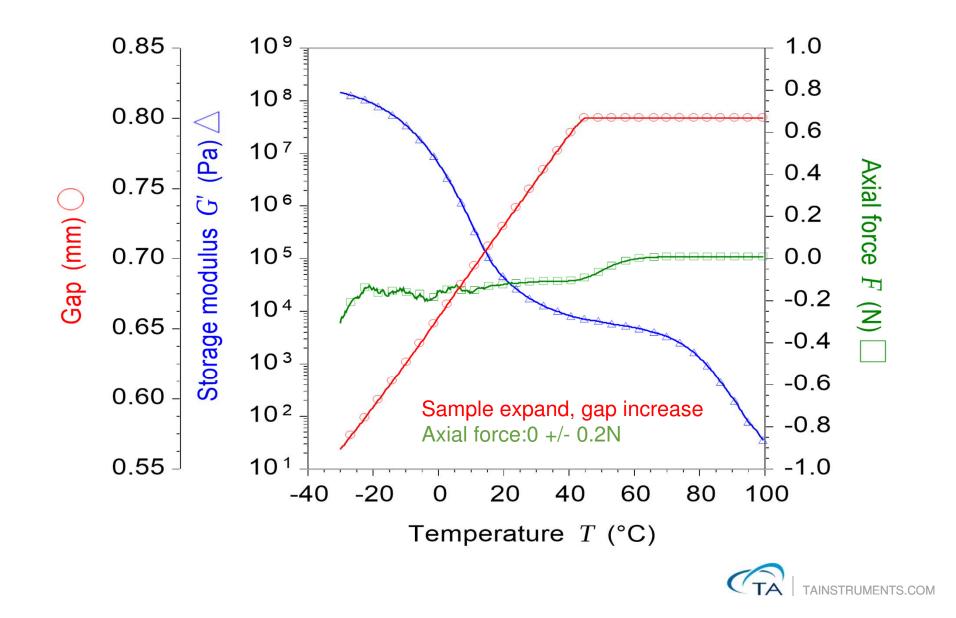
Temperature



Temperature Ramp of an Adhesive



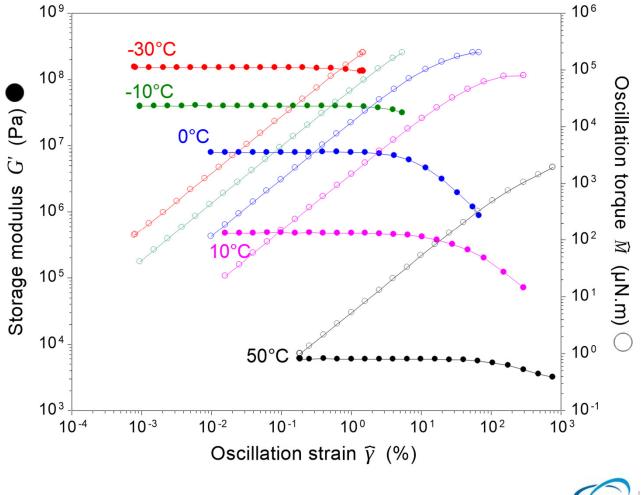
Using Axial Force Control in a Temp Ramp Test



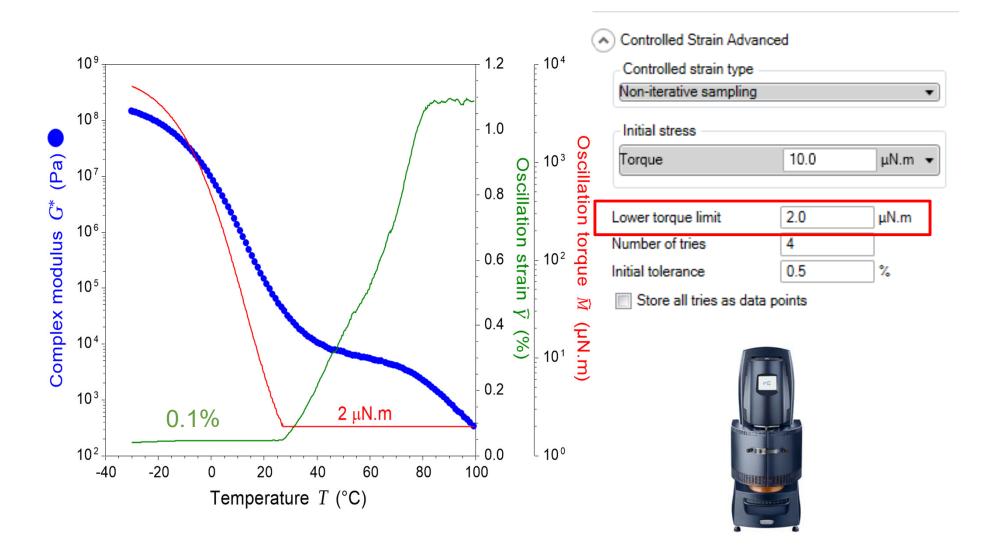
Adjusting strain and torque in temperature ramp

@ Low temperature:A small strain is preferred.

@ High temperature:A large strain is preferred.

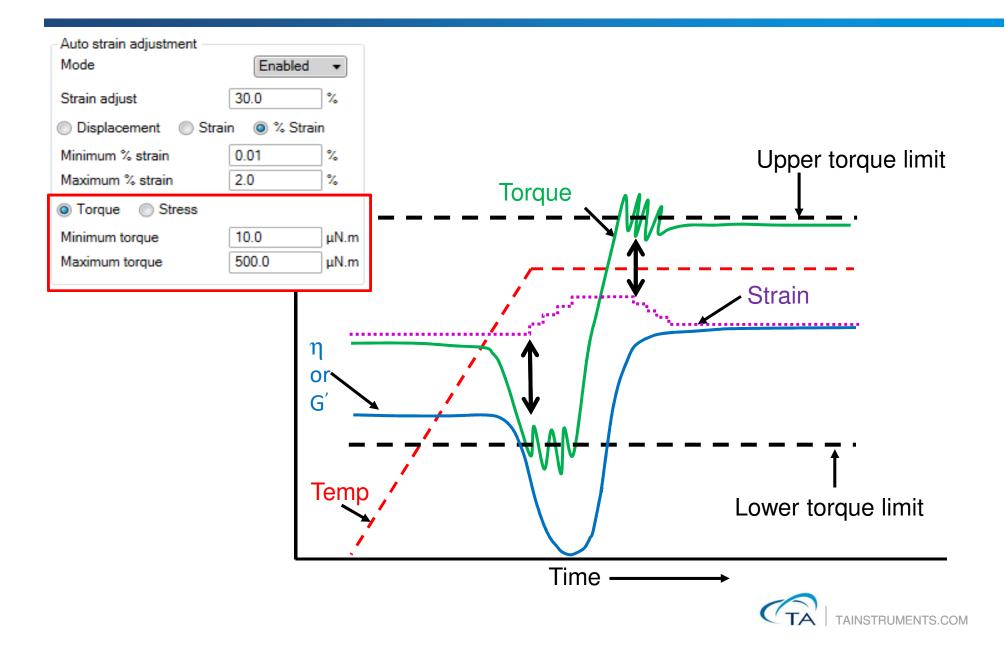


DHR and AR: Non-iterative Sampling

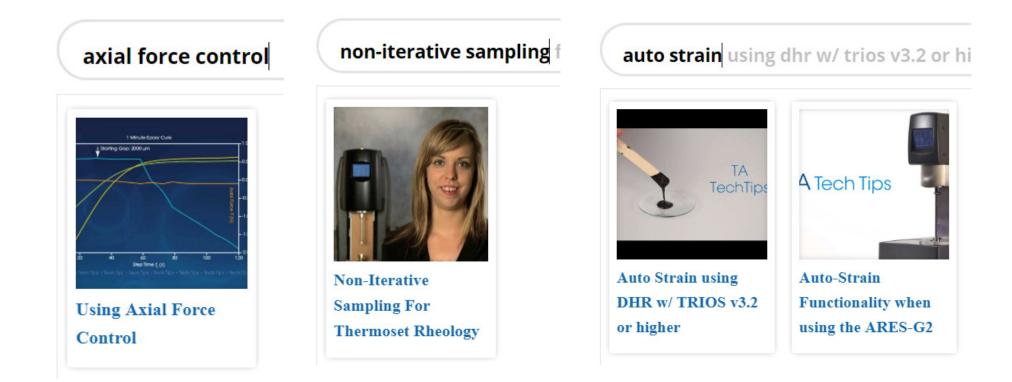




ARES-G2 and DHR: Auto-Strain



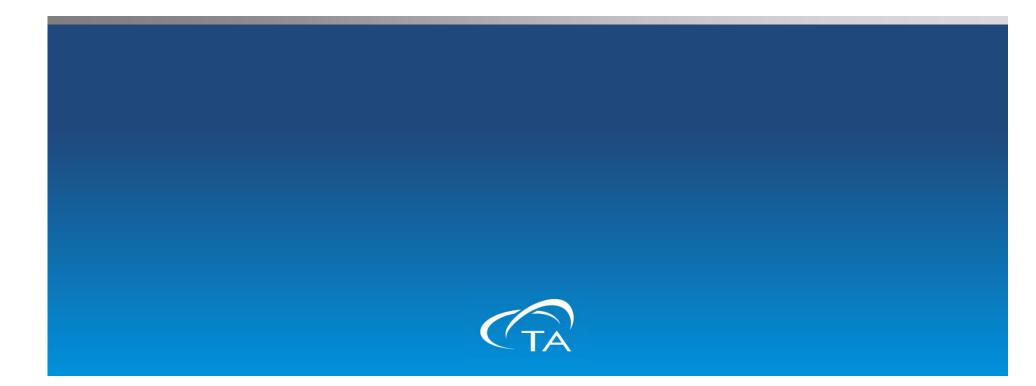
TA Tech tips



 Videos available at <u>www.tainstruments.com</u> under the Videos tab or on the TA tech tip channel of YouTube[™] (<u>https://www.youtube.com/user/TATechTips</u>)

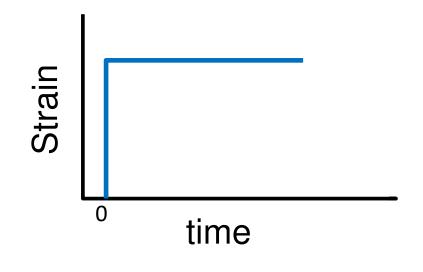


Setting up Rheological Experiments Transient Tests



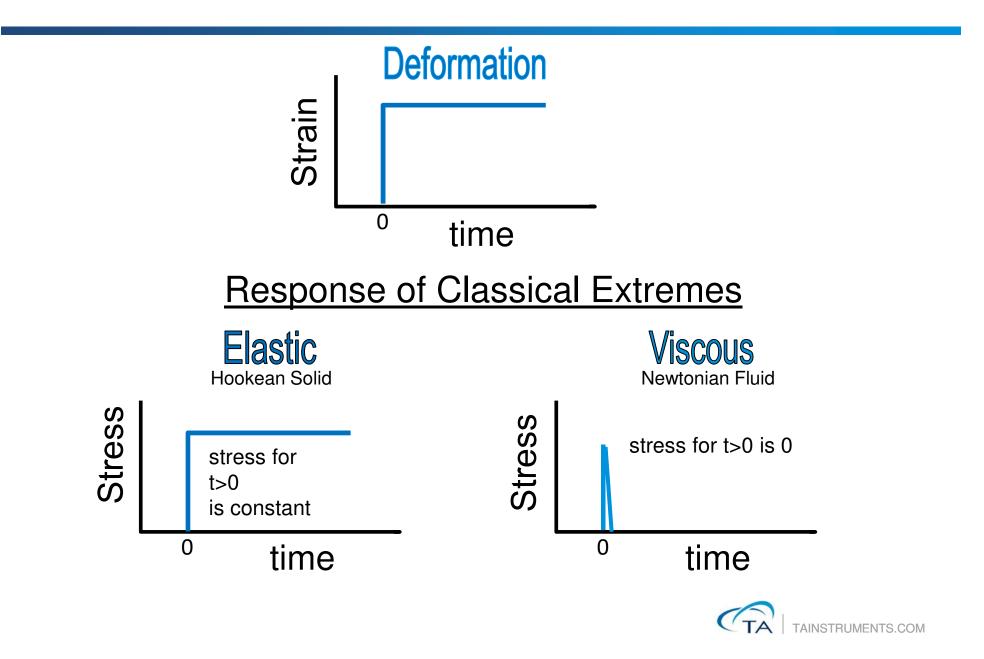
Stress Relaxation Experiment

- Strain is applied to sample instantaneously (in principle) and held constant with time.
- Stress is monitored as a function of time $\sigma(t)$.





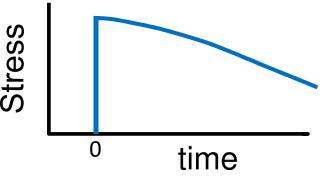
Stress Relaxation Experiment



Stress Relaxation Experiment

Response of ViscoElastic Material

Stress decreases with time starting at some high value and decreasing to zero.



- For small deformations (strains within the linear region) the ratio of stress to strain is a function of time only.
- This function is a material property known as the STRESS RELAXATION MODULUS, G(t) G(t) = σ(t)/γ



Determining Strain For Stress Relaxation

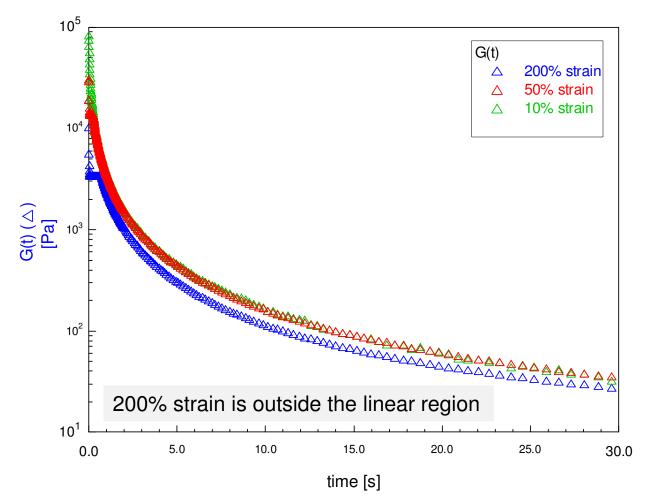
- Research Approach, such as generation of a family of curves for TTS, then the strain should be in the linear viscoelastic region. The stress relaxation modulus will be independent of applied strain (or will superimpose) in the linear region.
- Application Approach, mimic real application. Then the question is "what is the range of strain that I can apply on the sample?" This is found by knowing the Strain range the geometry can apply.
 - The software will calculated this for you.

 $\gamma = K_{\gamma} \times \Theta$ (% $\gamma = \gamma \times 100$)



Stress Relaxation and Linear Region

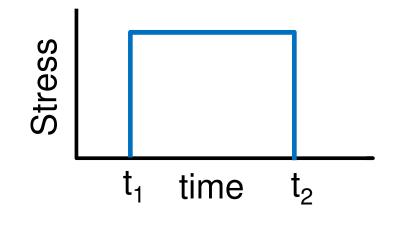
Stress Relaxation of PDMS, Overlay





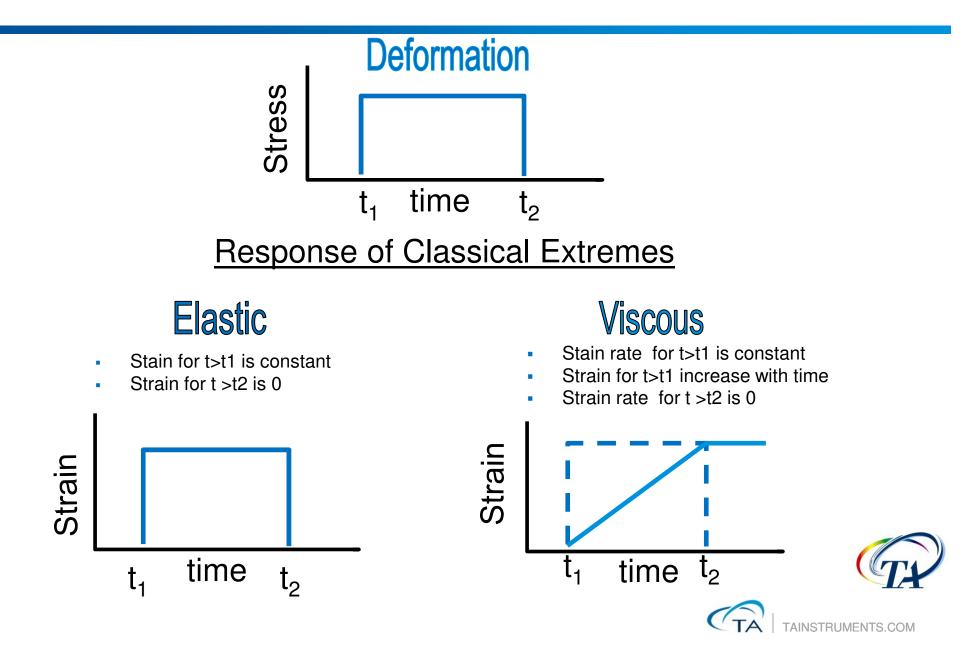
Creep Recovery Experiment

Stress is applied to sample instantaneously, t₁, and held constant for a specific period of time. The strain is monitored as a function of time (γ(t) or ε(t))
The stress is reduced to zero, t₂, and the strain is monitored as a function of time (γ(t) or ε(t))

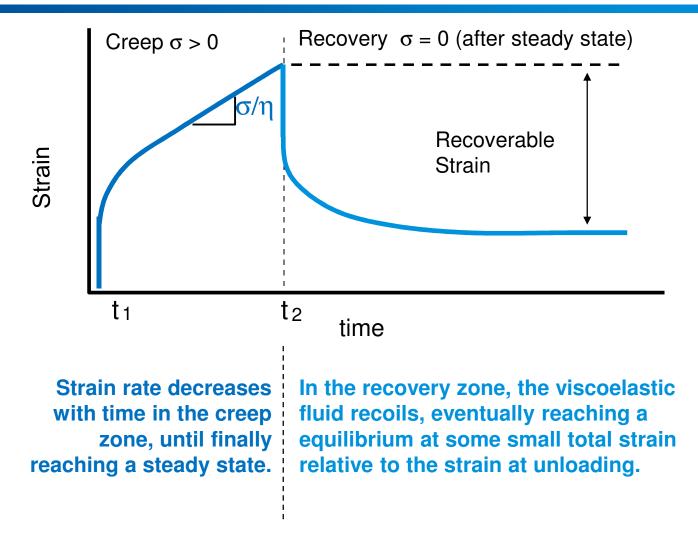




Creep Recovery Experiment



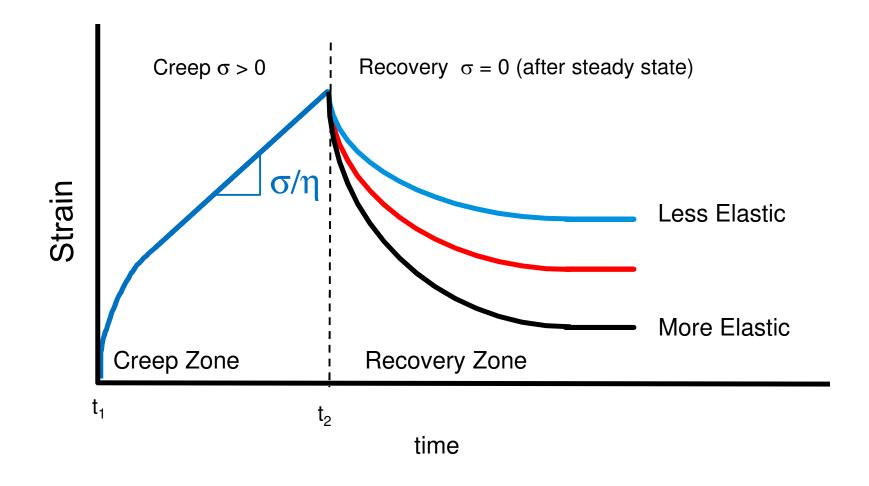
Creep Recovery: Response of Viscoelastic Material



Mark, J., et. al., Physical Properties of Polymers, American Chemical Society, 1984, p. 102.

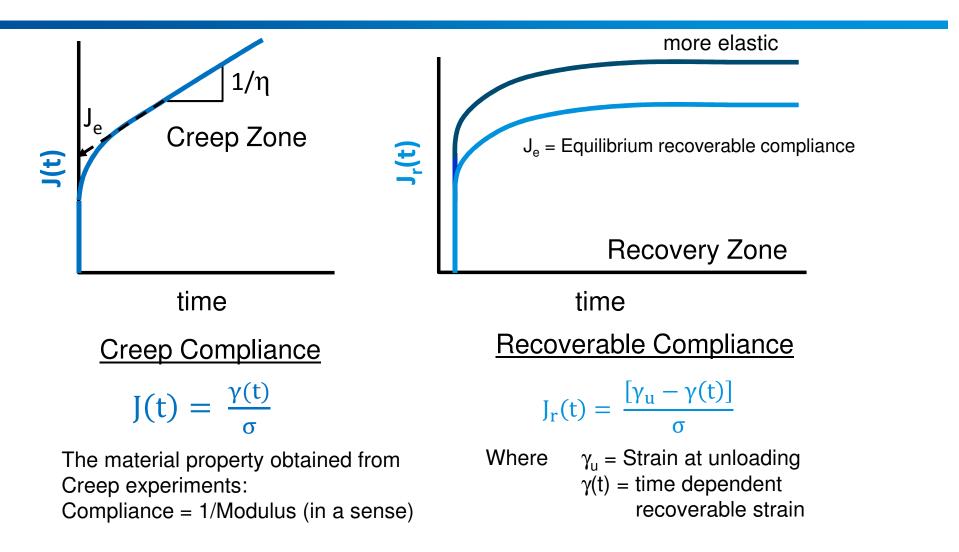


Creep Recovery Experiment





Creep Recovery : Creep and Recoverable Compliance



Mark, J., et. al., <u>Physical Properties of Polymers</u>, American Chemical Society, 1984, p. 102.



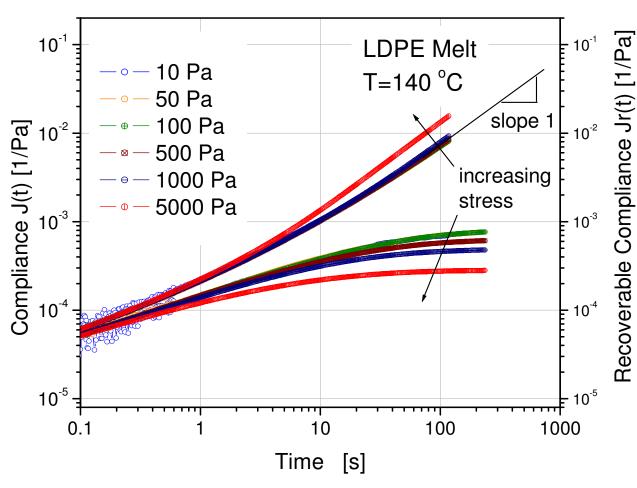
Determining Stress For Creep Experiment

- Research Approach If you are doing creep on a polymer melt, and are interested in viscoelastic information (creep and recoverable compliance), then you need to conduct the test at a stress within the linear viscoelastic region of the material.
- Application Approach If you are doing creep on a solid, you want to know the dimension change with time under a specified stress and temperature, then the questions is "what is the max/min stress that I can apply to the sample?". This is found by knowing the Stress range the geometry can apply.
 - The software will calculated this for you.

 $\sigma = K_{\sigma} \times M$



Creep and Recovery with Increasing Stress

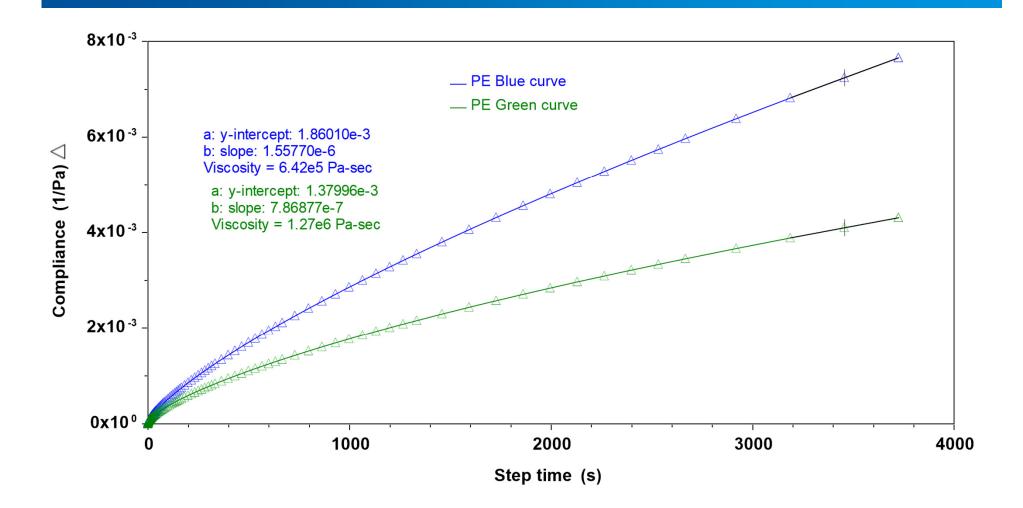


LDPE Melt creep recovery

Non linear effects can be detected in recovery before they are seen in the creep (viscosity dominates)



Creep Testing for Zero Shear Viscosity





Programming Creep on an ARES-G2

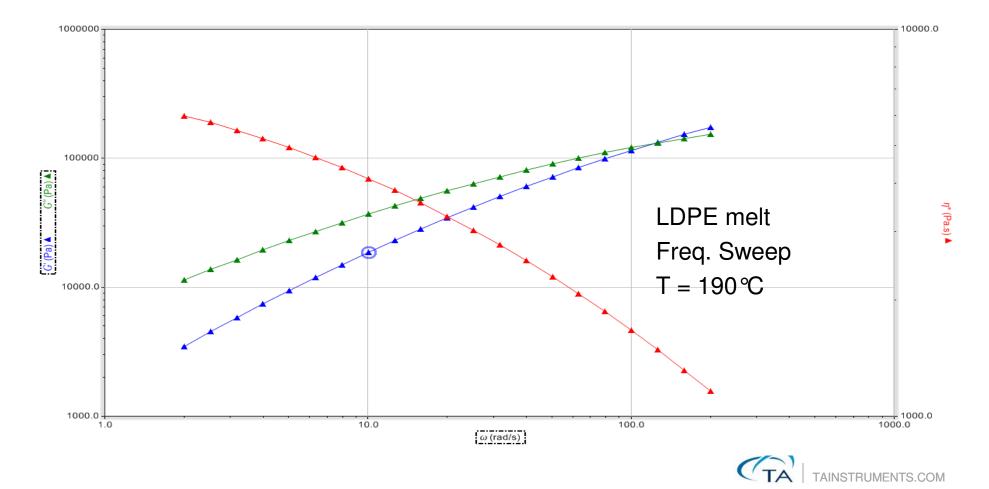
- Set up a pre-test and get the sample information into the loop
- Stress Control Pre-test: frequency sweep within LVR

[Experiment 2]	nly			
Geometry: Tension fixtu	re (rectangle)			
Procedure of 2 steps				S
 1: Conditioning Street 	ess Control			
Coad Precomput Environmental Co Temperature	-	and Calcul	ate	
Soak time	60.0	s	Wait for temperatu	ire
_ Test Parameters				
Strain %	0.05	%		~
Save stress con	trol PID file			
Stress control PID	file path: W:\201	1\creep.cre	ер	Save File
💉 Data acquisitio	n			



ARES-G2 Stress Control Pretest

Pretest \rightarrow Frequency Sweep from 2 to 200 rad/s \rightarrow data analyzed in software to optimize Motor loop control PID constants



Applications of Rheology Polymers



Purpose of a Rheological Measurement

Three main reasons for rheological testing:

- Characterization
 - MW, MWD, formulation, state of flocculation, etc.
- Process performance
 - Extrusion, blow molding, pumping, leveling, etc.
- Product performance
 - Strength, use temperature, dimensional stability, settling stability, etc.



Most Common Experiments on Polymers

Oscillation/Dynamic

- Time Sweep
 - Degradation studies, stability for subsequent testing
- Strain Sweep Find LVR
- Frequency Sweep G['], G["], η^{*}
 - Sensitive to MW/MWD differences melt flow can not see
- Temperature Ramp/Temperature Step
 - Transitions, end product performance
- TTS Studies

Flow/Steady Shear

- Viscosity vs. Shear Rate, mimic processing
- Find Zero Shear Viscosity
- Low shear information is sensitive to MW/MWD differences melt flow can not see

Creep and Recovery

 Creep Compliance/Recoverable Compliance are sensitive to long chain entanglement, elasticity



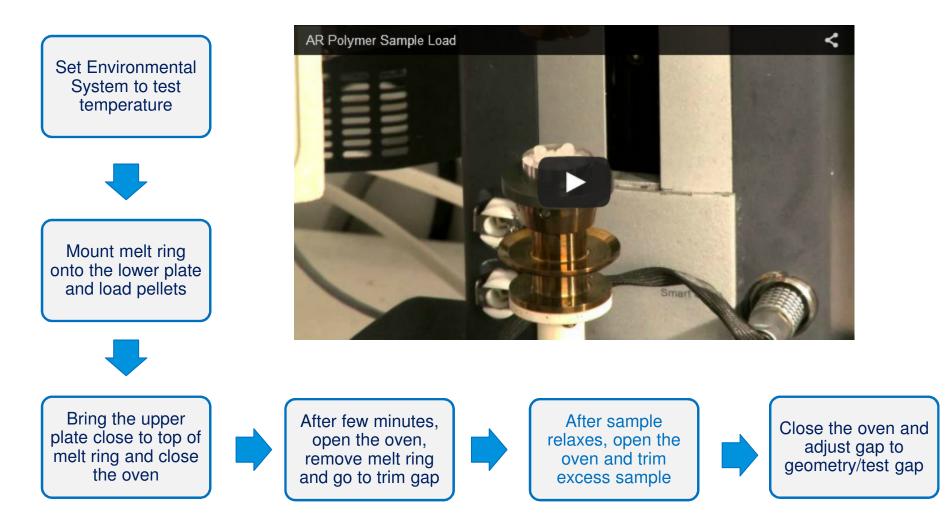
Know Your Sample – Polymers



- Polymer samples come in different forms (e.g. powder, flakes, pellets) and can be sensitive to environmental conditions
- Careful sample preparation techniques are required to prepare good test specimens for reproducible results
 - Molding a sample and punching discs
 - Handling powders, flakes
 - Controling the environment

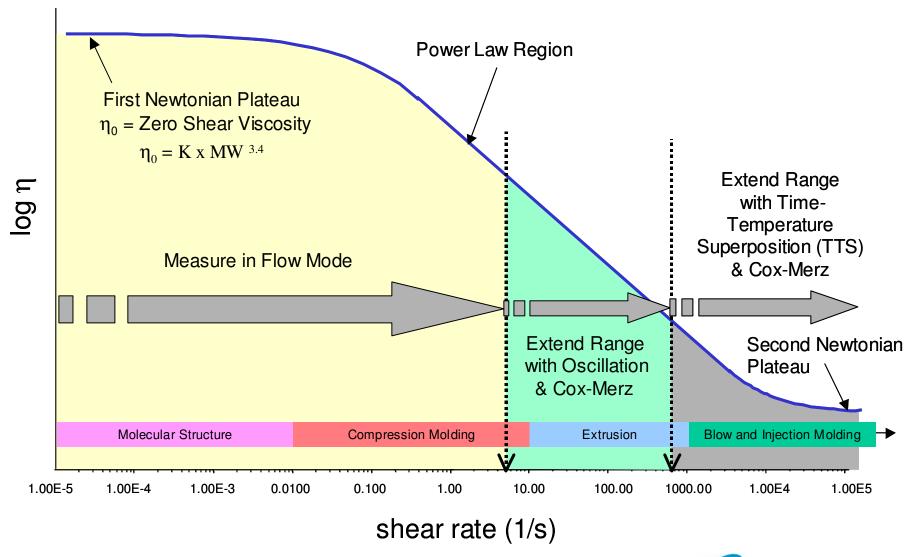


Loading Polymer Pellet Samples



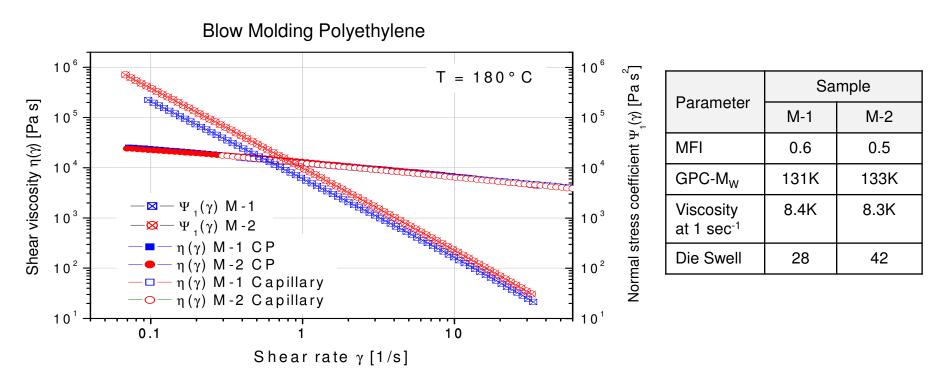


Idealized Flow Curve – Polymer Melts





Effect of HDPE Variations in Blow Molding



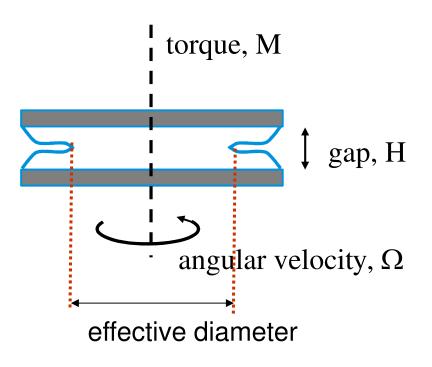
No differences in MFI, Viscosity, or GPC!

M-2 produces heavier bottles in blow molding due to increased parison swell



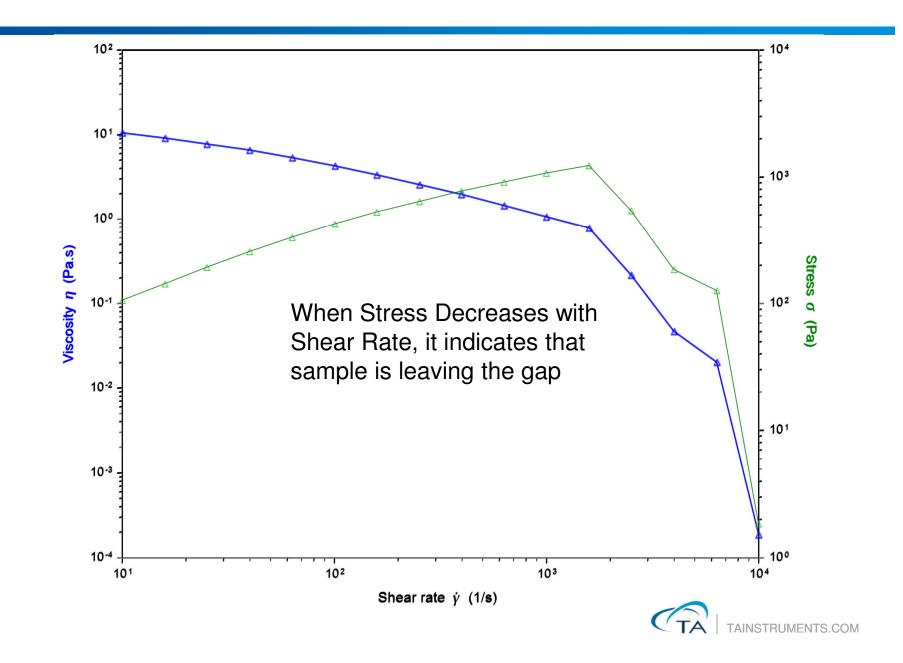
Edge Fracture

- Edge fracture is caused by the elasticity of the fluids
- •When shearing a viscoelastic material, a large normal stress difference (created from its elasticity) can lead to a crack formation at the geometry edge. This is called edge fracture.
- Results: decrease in viscosity
- To minimize edge fracture
 - Decrease measurement gap
 - Use partitioned plate



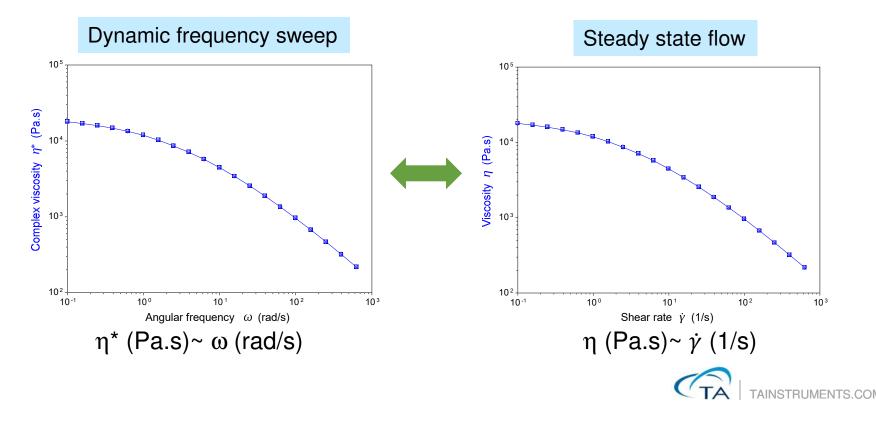


Shear Thinning or Sample Instability?



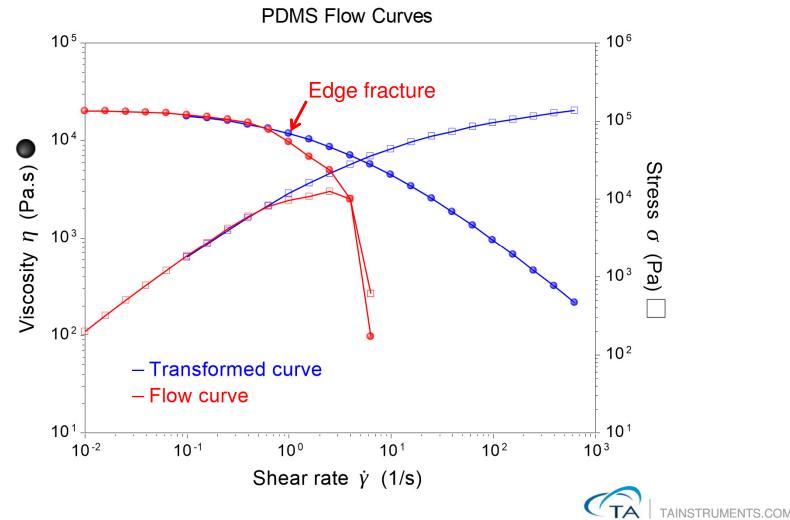
The Cox-Merz Rule

- For materials that exhibit wall slip or edge fracture, one alternative way to obtain viscosity information over shear is to use the Cox-Merz rule
- Cox-Merz "rule" is an empirical relationship. It was observed that in many polymeric systems, the steady shear viscosity plotted against shear rate is correlated with the complex viscosity plotted against frequency



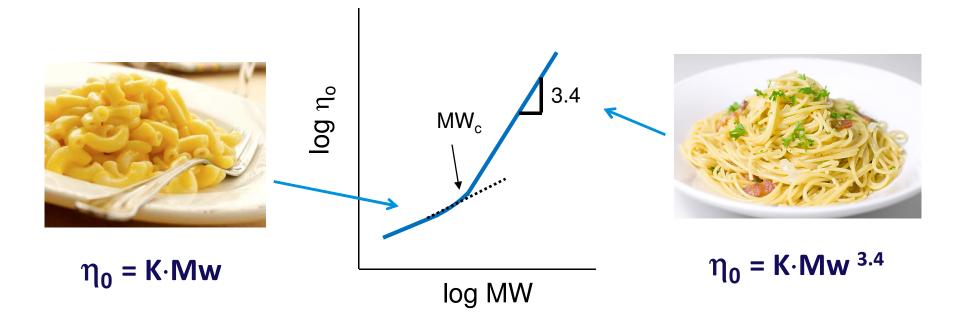
Cox-Merz Transformation Benefit

The Cox-Merz transformation works primarily with polymer melts and polymer solutions



Melt Rheology: MW Effect on Zero Shear Viscosity

- Sensitive to Molecular Weight, MW
- For Low MW (no Entanglements) η_0 is proportional to MW
- For MW > Critical MW_c, η_0 is proportional to MW^{3.4}

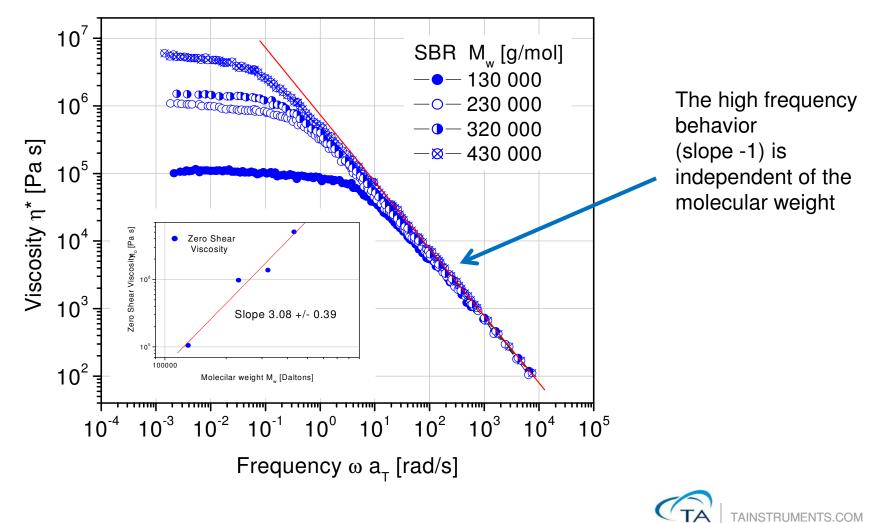


Ref. Graessley, Physical Properties of Polymers, ACS, c 1984.



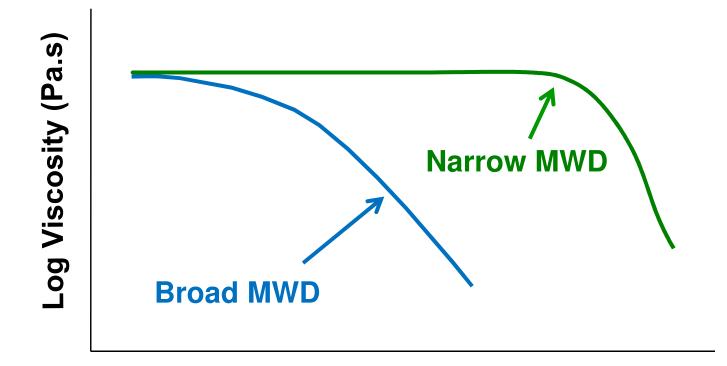
Influence of MW on Viscosity

The zero shear viscosity increases with increasing molecular weight. TTS is applied to obtain the extended frequency range.



Influence of MWD on Viscosity

• A Polymer with a broad MWD exhibits non-Newtonian flow at a lower rate of shear than a polymer with the same η_0 , but has a narrow MWD.

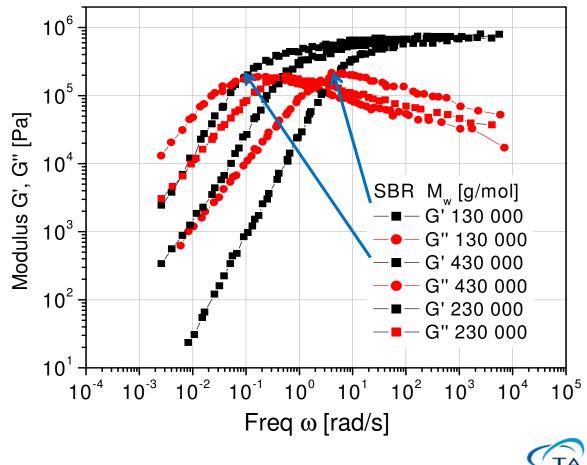


Log Shear Rate (1/s)

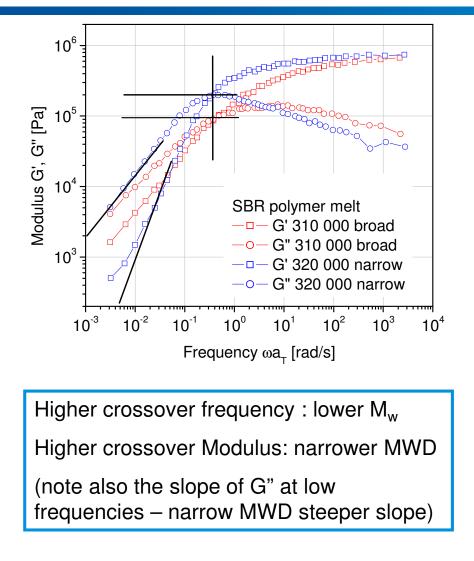


Influence of MW on G' and G"

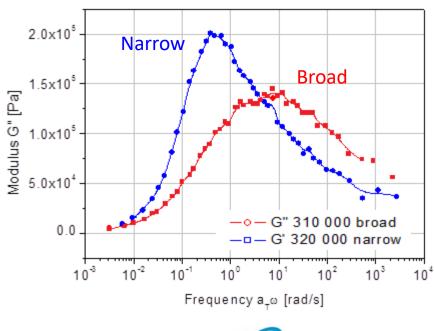
The G' and G" curves are shifted to lower frequency with increasing molecular weight.



Influence of MWD on G' and G"

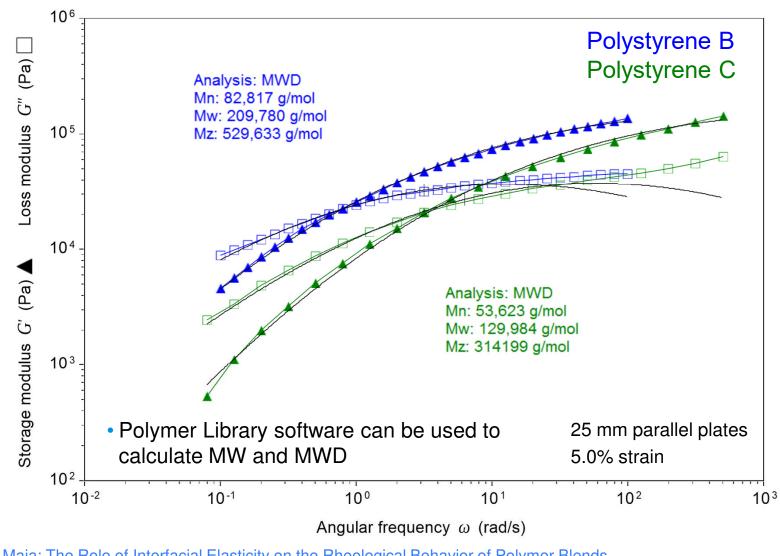


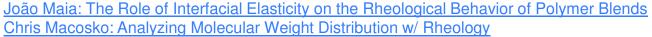
 The maximum in G" is a good indicator of the broadness of the distribution



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Frequency sweep - polymer melt (ASTM D4440)

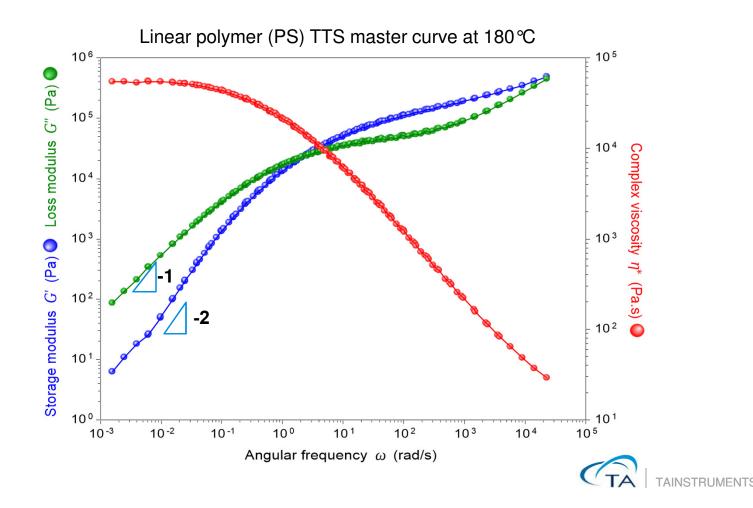




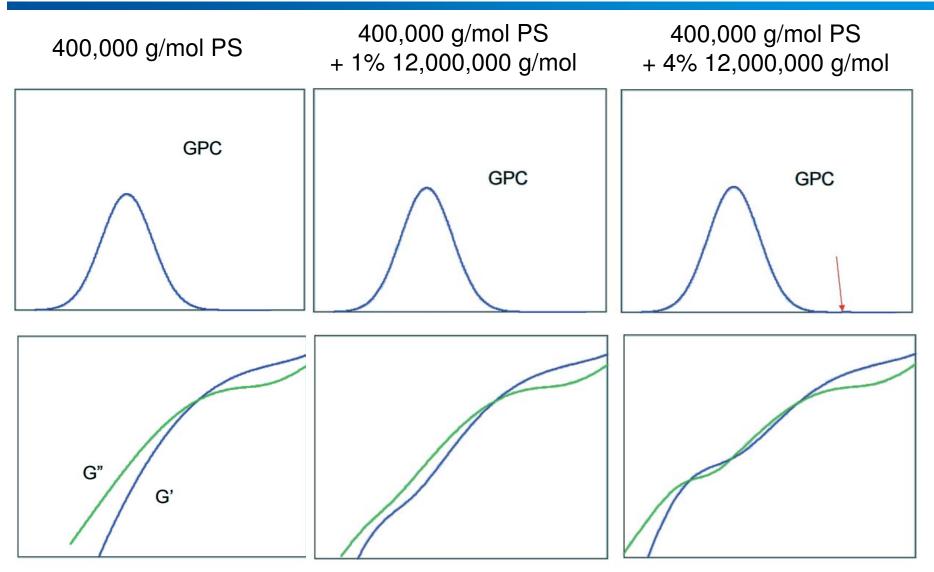


Frequency Sweep-Terminal Regime

- The terminal regime in a frequency sweep result is sensitive to polymer structure
- For a linear polymer:
 - G": straight line with slope of -1; G': straight line with slope of -2



High MW Contributions

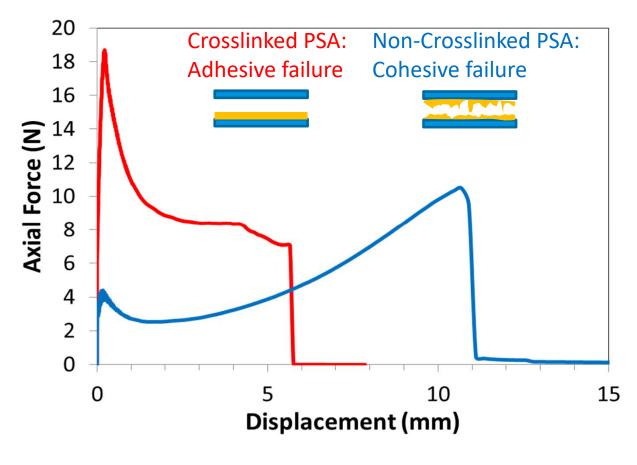


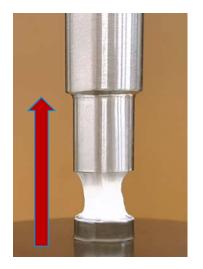
Macosko, TA Instruments Users' Meeting, 2015



Adhesive Tack Testing

- Tack testing method: ASTM D2979
- Use 8mm parallel plate, axial tensile at 0.1mm/sec
- The maximum force required to pull the plate away is defined as the sample's tackiness.







Extensional Viscosity Measurements

- Non linear elongation flow is more sensitive for some structure elements (e.g. branching) than shear flows
- Many processing flows are elongation flows. Extensional viscosity measurements can be used to help predict processability

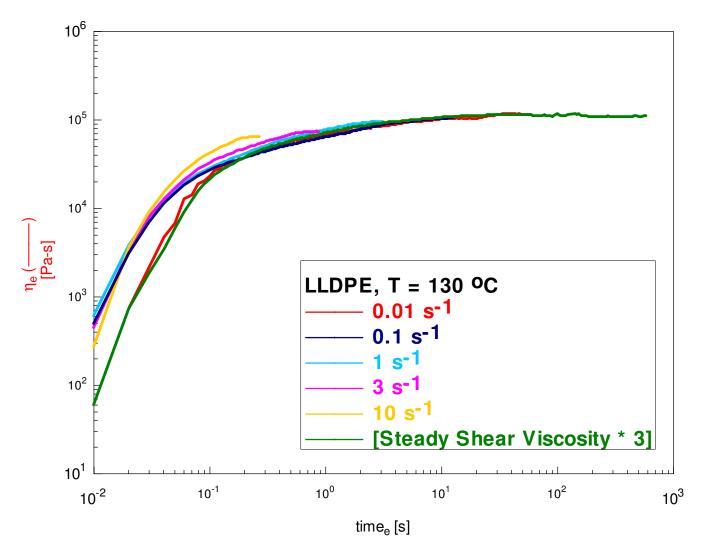






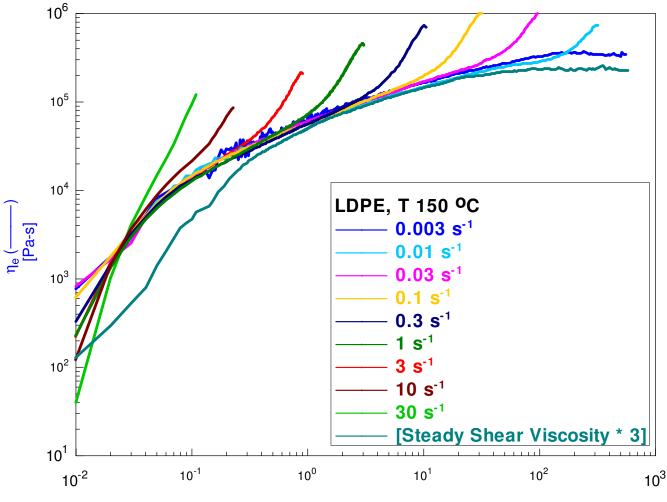


LLDPE (Low branching)





LDPE (High branching)







Thermosetting Polymers

 Thermosetting polymers are perhaps the most challenging samples to analyze on rheometers as they challenge all instrument specifications both high and low.

 The change in modulus as a sample cures can be as large as 7-8 decades and change can occur very rapidly.





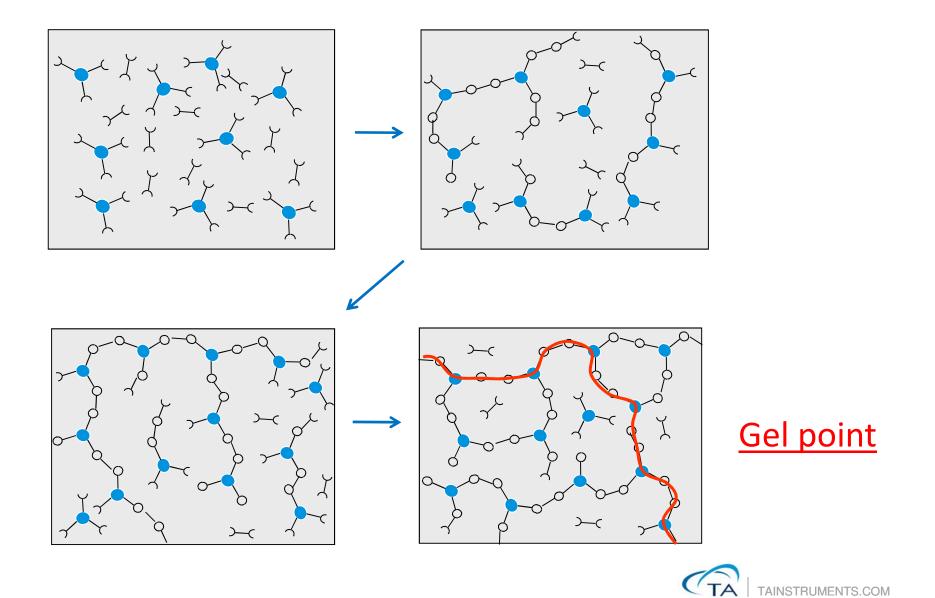


Thermosets Analysis

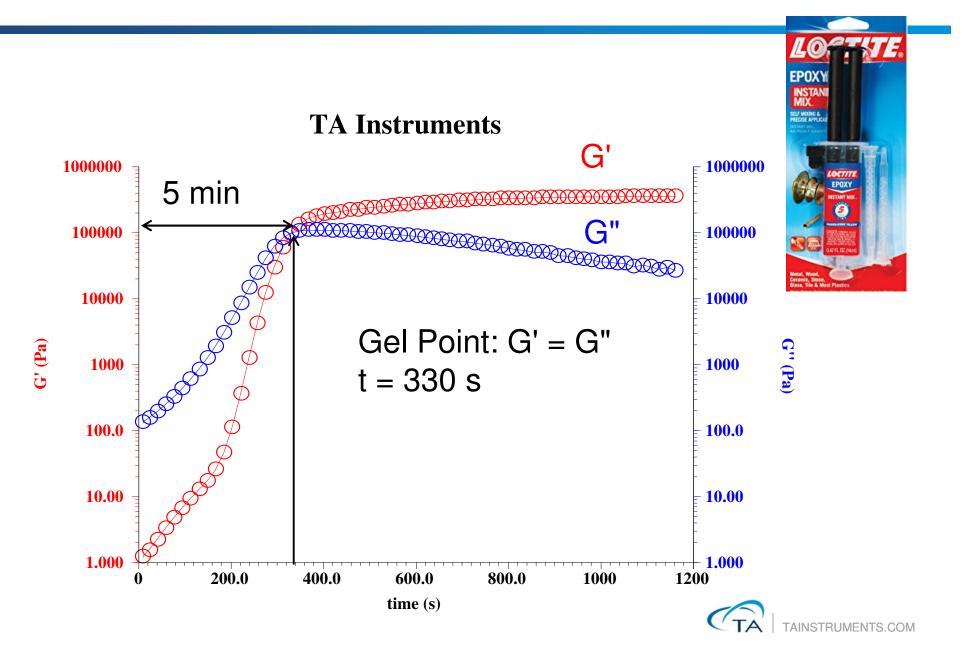
- Monitor the curing process
 - Viscosity change as function of time or temperature
 - Gel time or temperature
- Test methods for monitoring curing
 - Isothermal time sweep
 - Temperature ramp
 - Combination profile to mimic process
- Analyze cured material's mechanical properties (G', G', tan δ , T_g etc.)



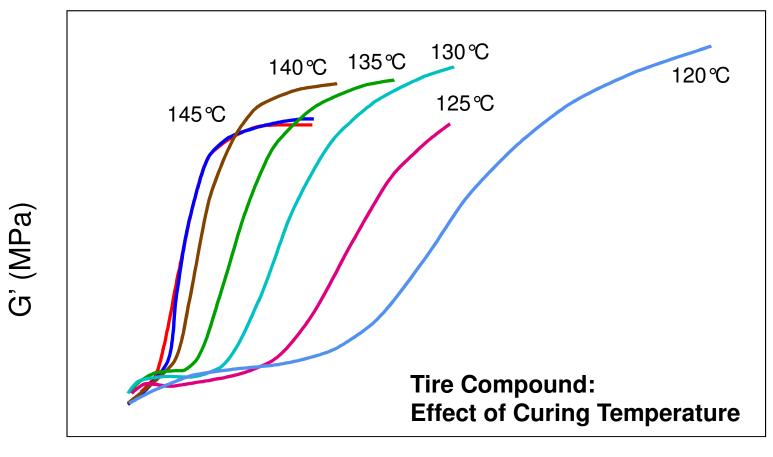
Structural Development During Curing



Curing Analysis: Isothermal Curing



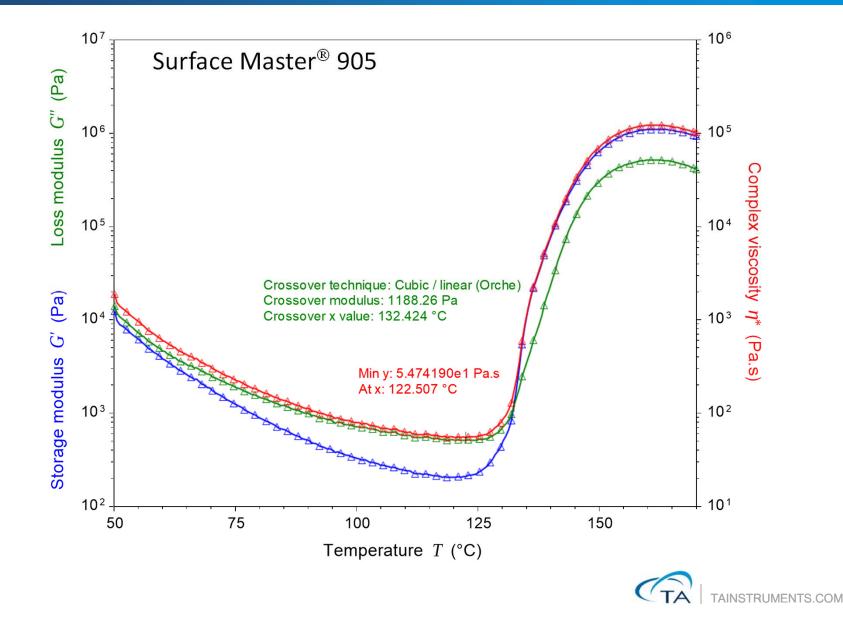
Isothermal Curing



Time (min)

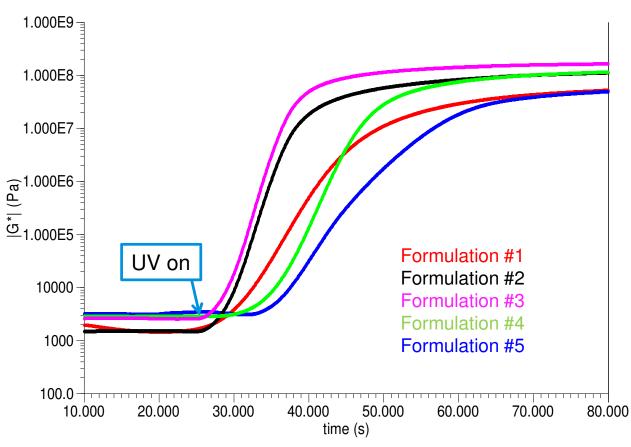


Temperature Ramp Curing



UV Curing

- Monitor UV curing: Dynamic time sweep
- Measure curing time with different formulations, UV intensity and temperature
- Measure cured adhesive modulus



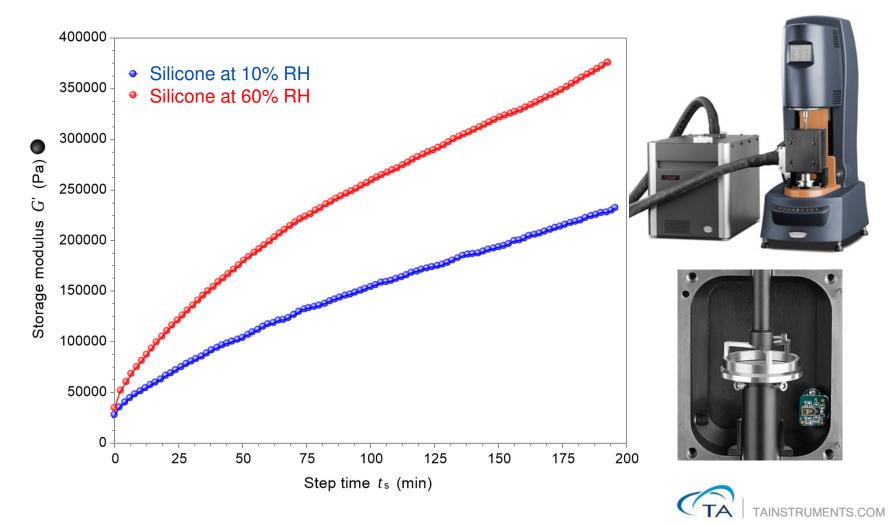






Curing with Controlled Humidity

- Silicone adhesive curing under 25 ℃ and 10%; 60% relative humidity
- Higher humidity, faster curing



Testing Solids: Torsion and DMA

- Torsion and DMA geometries allow solid samples to be characterized in a temperature controlled environment
 - Torsion measures G', G", and Tan δ
 - DMA measures E', E", and Tan δ
 - DMA mode on ARES G2 (max 50 μm amplitude)
 - DMA mode on DHR (max 100 μm amplitude)

E = 2G(1 + v)

v : Poisson's ratio



Torsion rectangular and cylindrical clamps

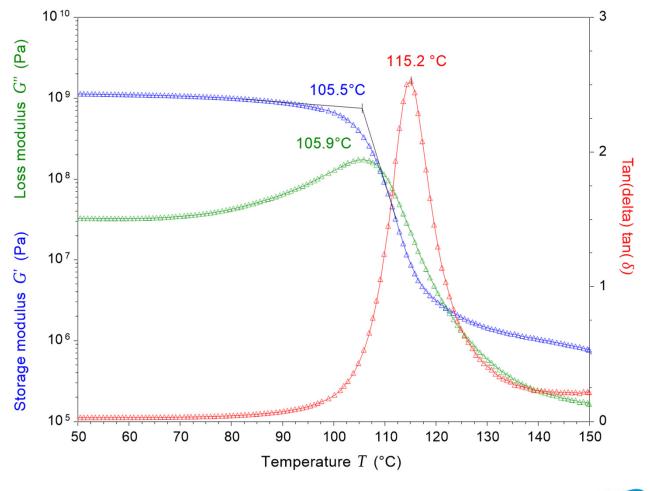


DMA cantilever, 3-point bending and tension clamps



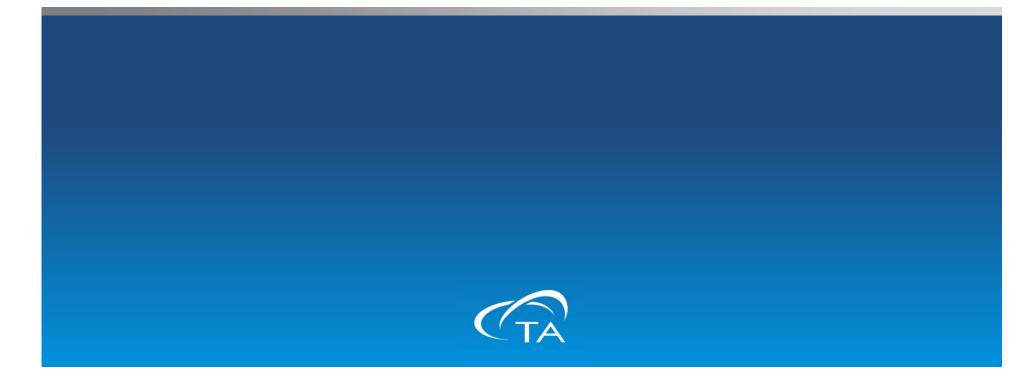
Dynamic Temp Ramp Test

• Measure moduli, tan δ and transitions



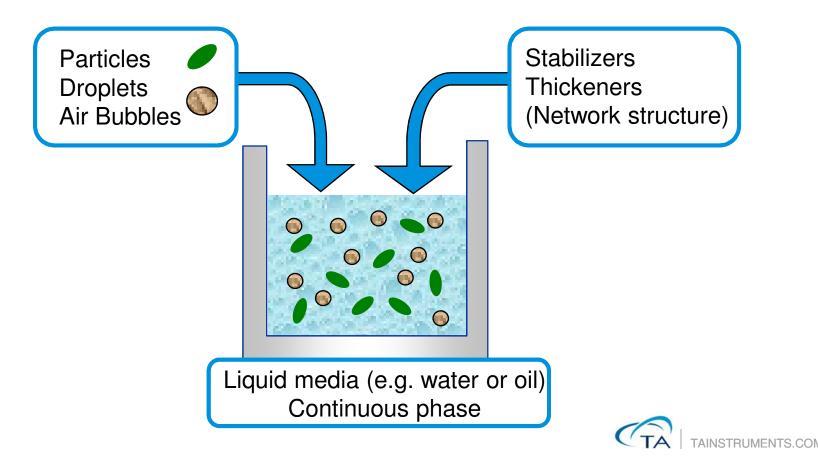


Applications of Rheology Yield stress and thixotropy of structured Fluids



Structured Fluids

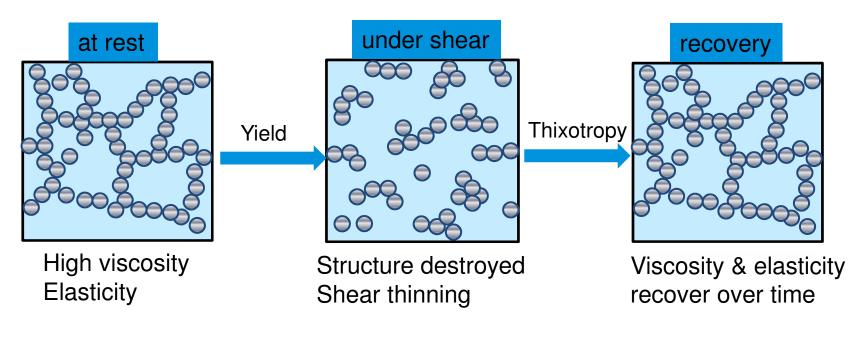
- •A multiphase complex system consists of a continuous phase (e.g. water or oil) and a dispersed phase (solid, fluid, gas)
- Stabilizers or thickeners are added to form a weak three dimensional network structure



Properties of Structured Fluids

Structured fluid properties

- Non-Newtonian
- Yield stress
- Thixotropic
- Viscoelasticity





Types of Structured Fluids

Three categories

Solid particles in a Newtonian fluid

• <u>Emulsion</u> Fluid in a fluid

• <u>Foam</u> Gas in a fluid (or solid)

• Examples are:

- Paints
- Coatings
- o Inks
- Adhesives
- Personal Care Products
- Cosmetics
- Foods



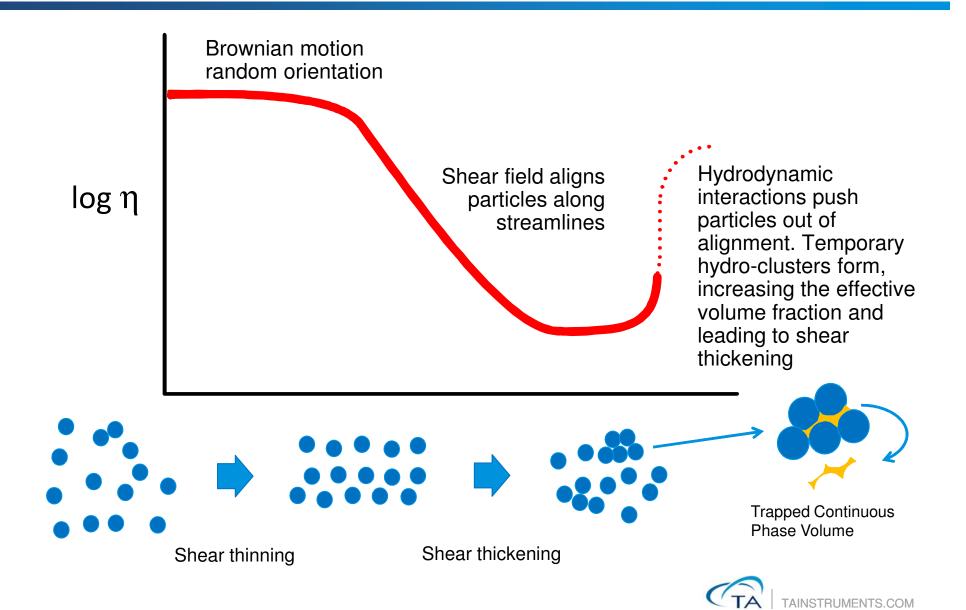






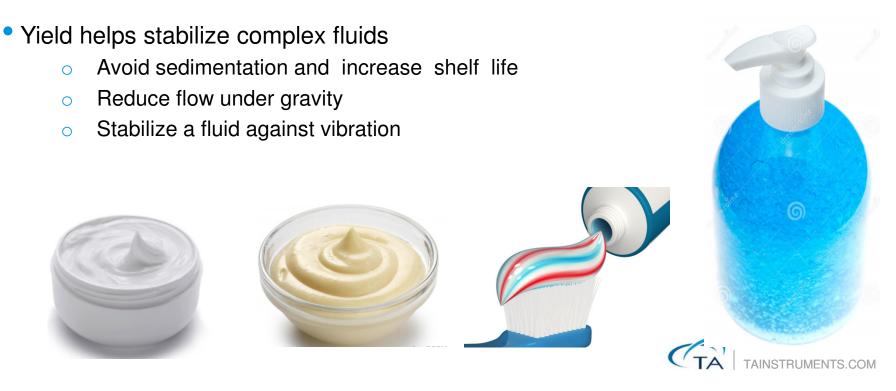


Generalized Flow Curve for structured fluids



What is Yield?

- Yield stress is a time dependent characteristic that is associated with many structured fluids such as Mayonnaise, Ketchup, hand lotion, hair gels, paints etc.
- A material that has yield does not flow unless the applied stress exceeds a certain value – yield point
- Yield stress is created in formulation by adding additional thickeners



How to Measure Yield

Yield can be quantitatively measured on a rotational rheometer

Common methods

Stress ramp
Stress sweep
Shear rate ramp
Dynamic stress/strain sweep

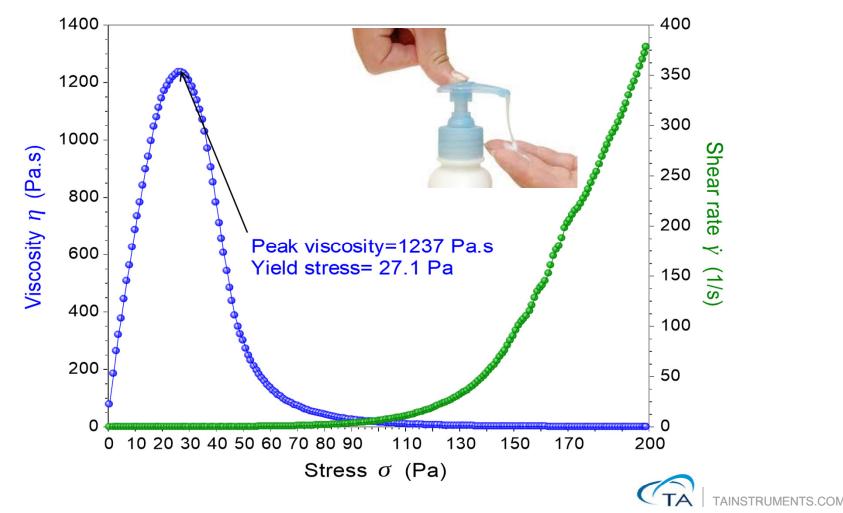
Note:

Yield behavior is a time dependent characteristic. Measured yield stress values will vary depending on experimental parameters



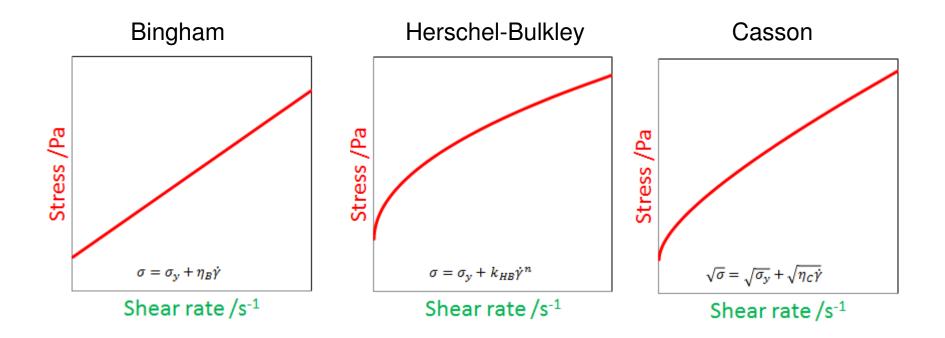
Yield Stress of a Body Lotion

- Stress ramp from 0 to 200 Pa in 60 seconds
- Yield is determined at the point where viscosity shows a peak



Fit Results with a Flow Models

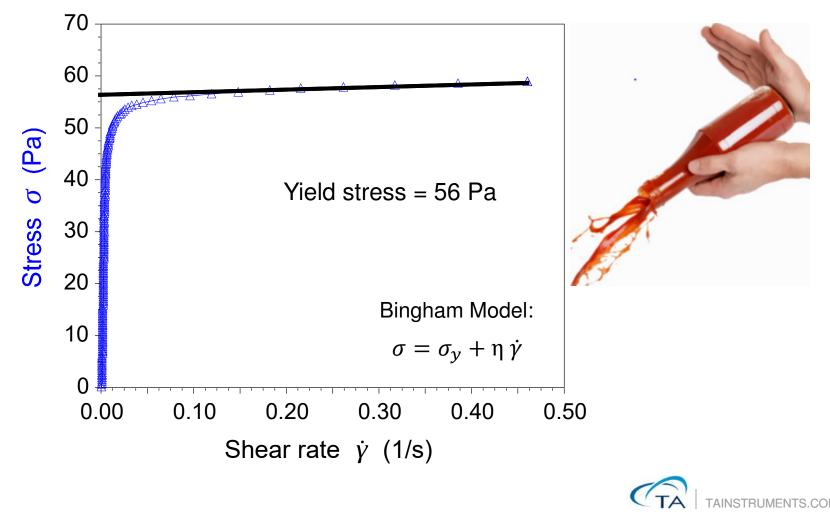
- Fit the stress ramp curves with a mathematical flow model
- Three flow models to describe the yield behavior





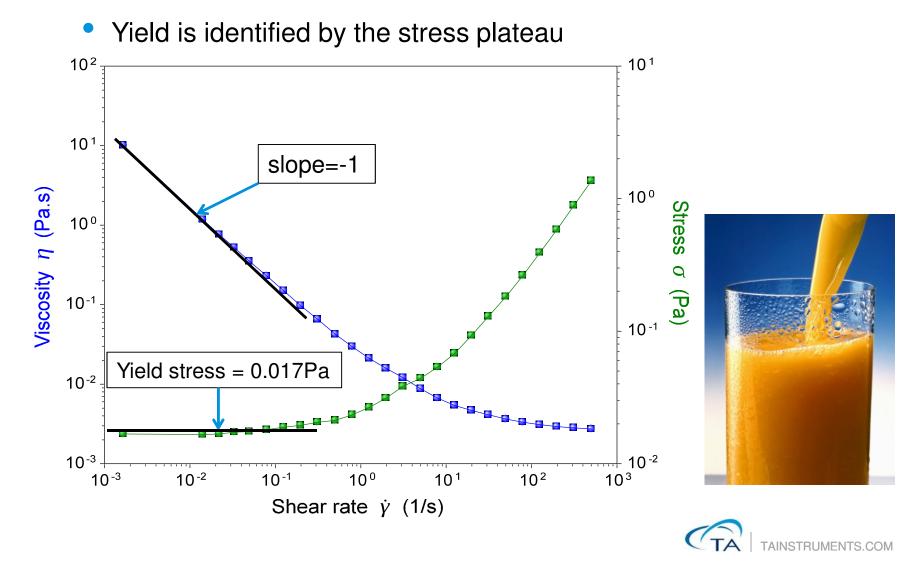
Yield Stress of Ketchup

- Stress ramp test on Katchup
- Yield is computed by fitting the flow curve with a mathematical model



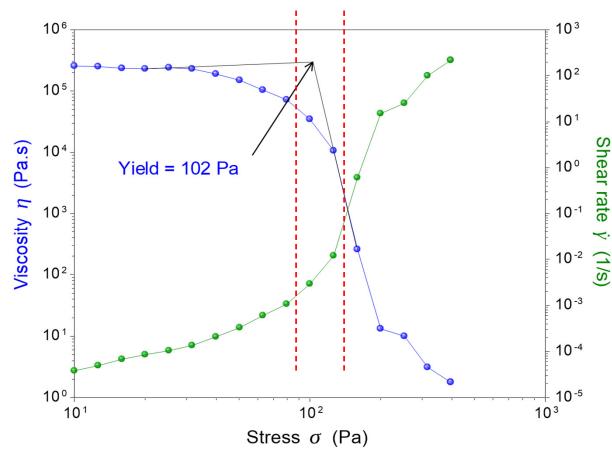
Yield Stress of Orange Juice

Shear rate ramp down from 500 to 0.001 1/s



Yield Stress of a Toothpaste

- Steady state stress sweep from 10 Pa to 500 Pa
- Yield stress is determined by a sharp decrease in viscosity over a narrow range of applied shear stress
- Take the onset of viscosity vs. stress curve



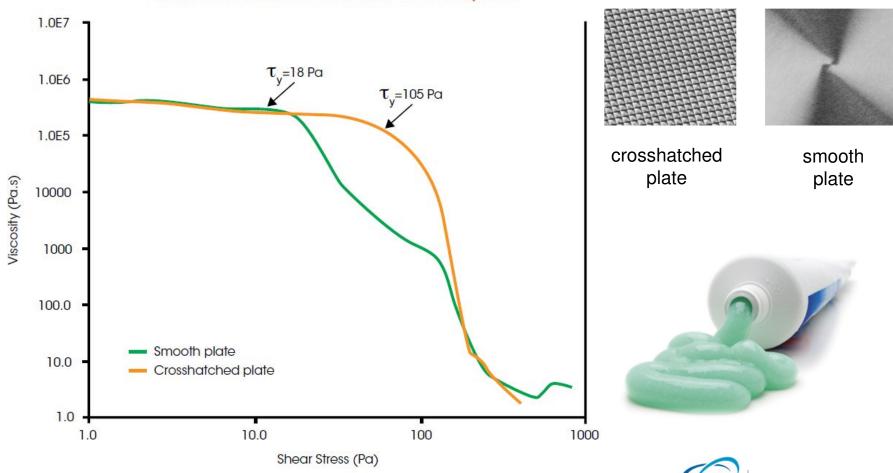






Wall Slip – Artifact Yield

- Incidence of wall slip is often observed when testing structured fluids
- Wall slip shows artifact yield



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Yield Stress Measurements on Toothpaste

Solutions To Minimize Wall Slip

Diagnosis method

 Running the same experiment at different gaps. For samples that don't slip, the results will be independent of the gap

Solutions

Use a grooved cup with vane or helical shape rotor geometry

Use a roughened surface geometry



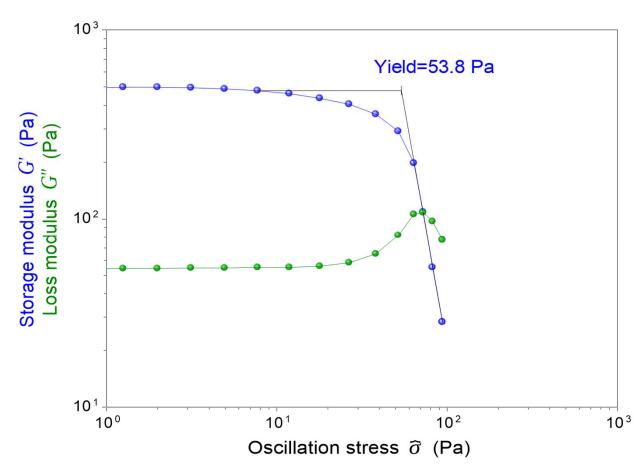






Yield Stress of Mayonnaise

- Dynamic stress/strain sweep test on Mayonnaise
- Yield stress is signified at the onset of G' vs. stress curve
- Yield determined by this method indicates the critical stress at which irreversible plastic deformation occurs







What is Thixotropy?

 Thixotropy is a time-dependent shear thinning property, which is used to characterize structure change reversibility

- A thixotropic fluid takes a finite time to attain equilibrium viscosity when introduced to a step change in shear rate
- Thixotropy is a desired property for many applications such as:

 Control sagging and levelling of paints
 Start up of pipleline flow after rest









How to Measure Thixotropy

 Thixotropy can be quantitatively measured on a rotational rheometer

Common methods

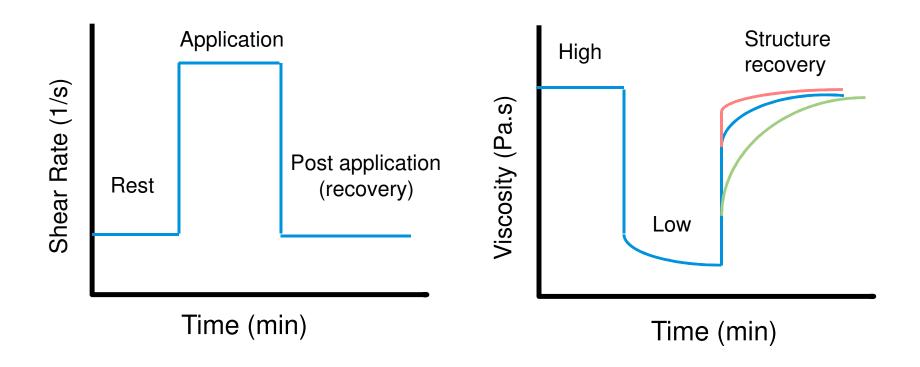
Stepped flow method
Stepped dynamic method
Stress ramp up and down method (Thixotropic loop)
Dynamic time sweep after pre-shear method

Note:

Thixotropic behavior is a time dependent characteristic. Measured thixotropy will vary depending on experimental parameters.



Stepped Flow Method



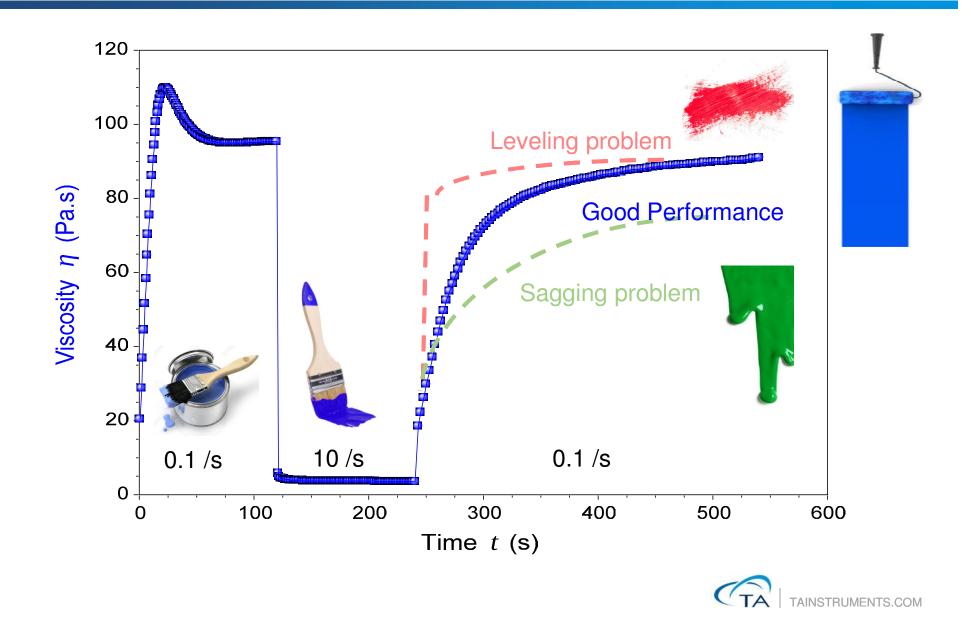
Experimental:

Step 1: Low Shear (e.g. 0.1 1/s), state of rest Step 2: High Shear (e.g. 10 1/s), structural destruction

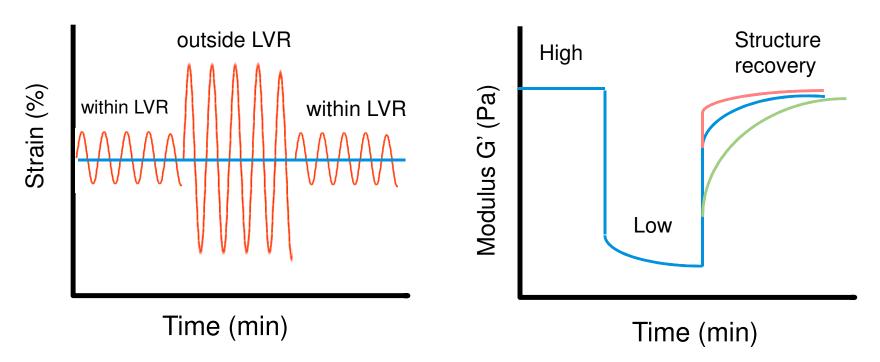
Step 3: Low Shear (e.g. 0.1 1/s), structural regeneration



Thixotropic Analysis of a Blue Paint



Stepped Dynamic Method



Experimental:

Step 1: Dynamic time sweep within LVR, structure at rest

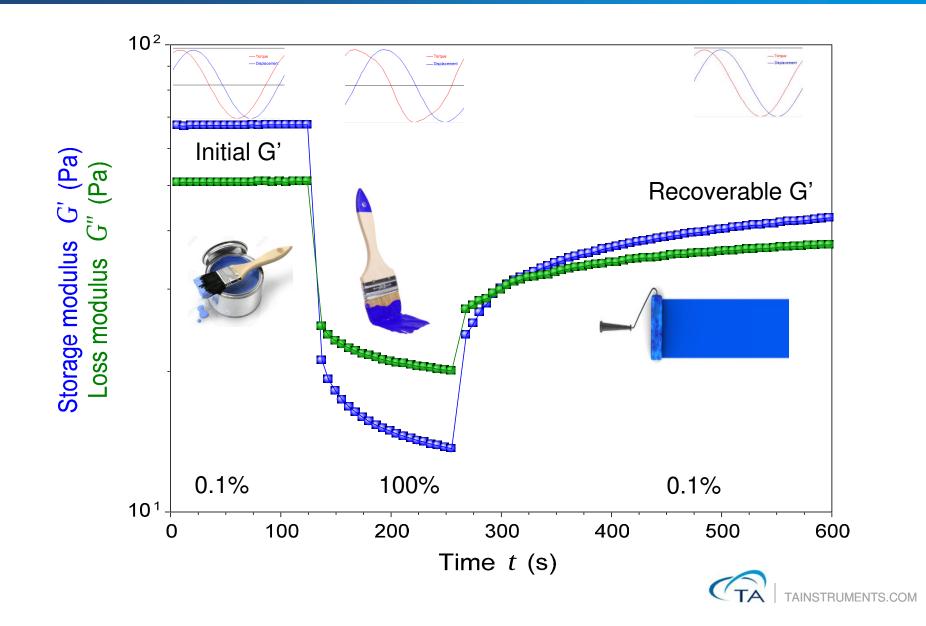
Step 2: Dynamic time sweep outside LVR, structural destruction

Step 3: Dynamic time sweep within LVR, structural regeneration

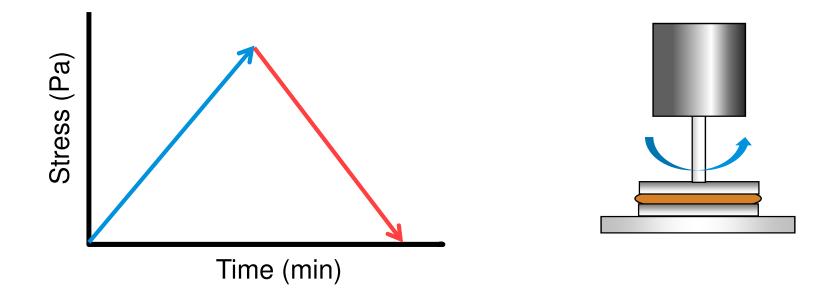
Good for measuring high viscosity samples



Blue Paint: Stepped Time Sweep



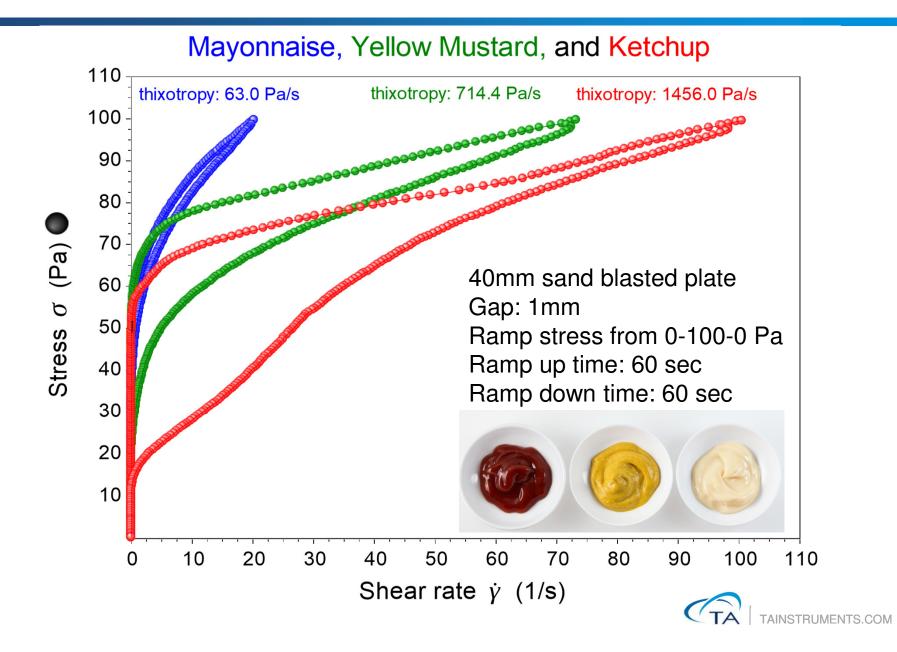
Stress Ramp Up and Down Method



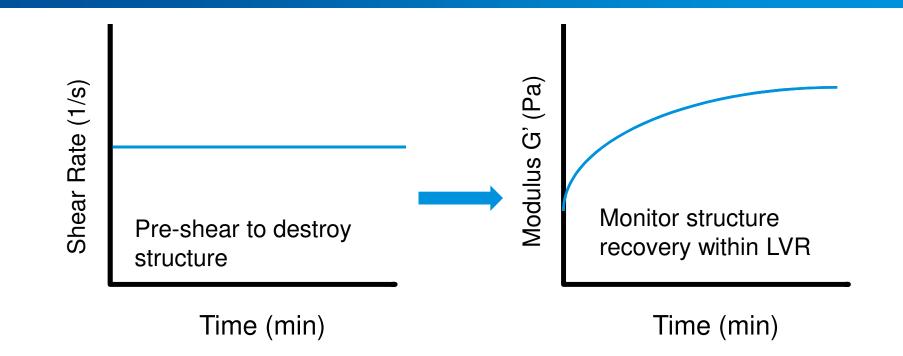
- Ramp shear stress linearly from zero up until sample flows, then ramp stress back down to zero
- Thixotropic index is measured by taking the area between the up and down stress curves
- •TA Tech Tip: <u>https://www.youtube.com/watch?v=8lZangOp1SY</u>



Thixotropic Loop Testing on Foods



Time Sweep After Pre-shear Method

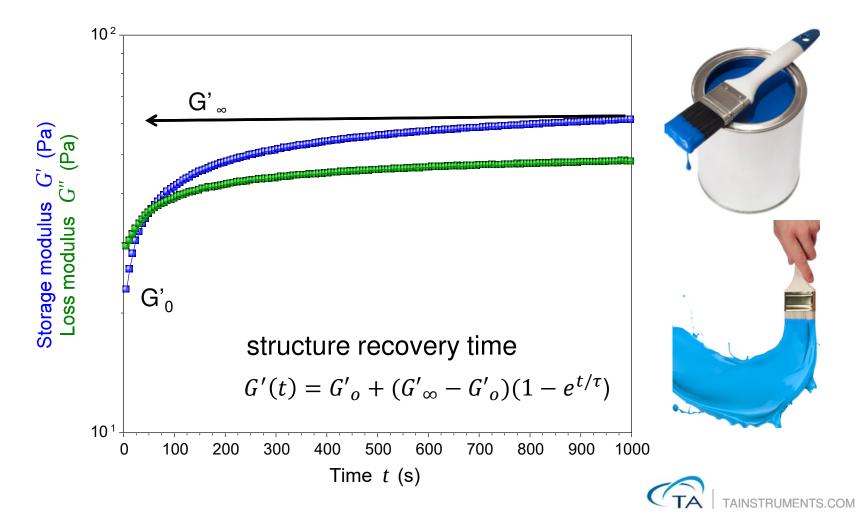


- Apply a constant shear (e.g. 10 or 100 1/s) for a certain time (e.g. 1 min.) to break down structure
- Immediately start a time sweep within the linear region of the material to monitor structure recovery



Blue Paint: Time Sweep After Pre-shear

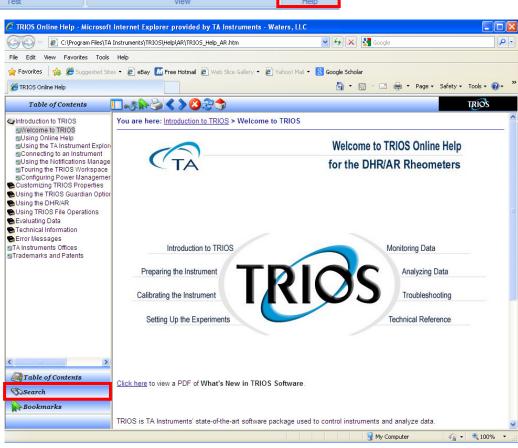
- Monitor the increase of the G' as a function of time.
- Thixotropic recovery is described by meausring the recovery time (τ)



TRIOS Help Menu



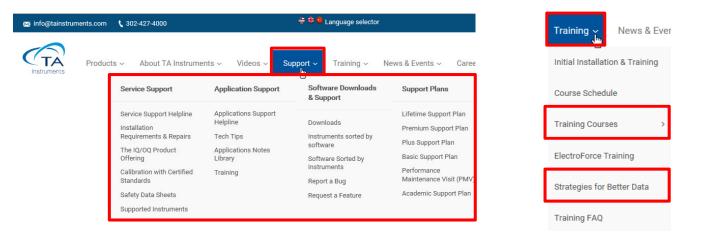
- Browse the contents list or search using the search tab.
- Access to <u>Getting Started</u> <u>Guides</u> also found through the help menu.



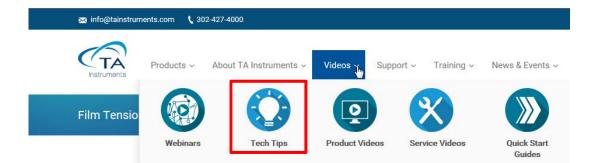


Instructional Videos

From <u>www.tainstruments.com</u> click on Videos, Support or Training



Select Videos for TA Tech Tips, Webinars and Quick Start Courses



See also: <u>https://www.youtube.com/user/TATechTips</u>



Instructional Video Resources

Quickstart e-Training Courses Strategies for Better Data - Rheology

Thermal Analysis

Rheology

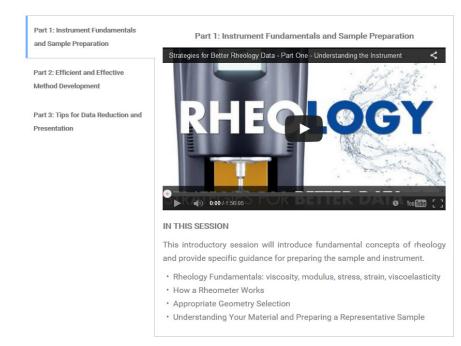
Web based e-Training Courses

TA Instruments offers a variety of training opportunities via the Internet. e-Training opportunities include the following:

QUICKSTART e-TRAINING COURSES

QuickStart e-Training courses are designed to teach a new user how to set up and run samples on their analyzers. These 60-90 minute courses are available whenever you are. These pre-recorded courses are available to anyone at no charge. Typically these courses should be attended shortly after installation.

Training ~	News & Events 🗸 Careers 🗸		
Initial Installatio	n & Training		
Course Schedul	e	Home / Trainir	
Training Courses		Theory & Applications	
ElectroForce Tr	aining	Courses	
Strategies for B	etter Data	Hands-On Training Courses	
Training FAQ		Custom Onsite Training Courses	
		Web based e-Training Coulmes	





Avoid Testing Artifacts

•TA Webinar - Professor Randy H. Ewoldt

http://www.tainstruments.com/randy-h-ewoldt-experimental-challenges-ofshear-rheology-how-to-avoid-bad-data-2/

About the Speaker

Randy H. Ewoldt is an Assistant Professor in the Department of Mechanical Science and Engineering at the University of Illinois at Urbana-Champaign. He has Ph.D. and S.M. degrees from MIT, and a B.S. degree from Iowa State, all in Mechanical Engineering. Before joining Illinois, he held a post-doctoral fellowship at the University of Minnesota. At Illinois, his research group studies rheology, fluid mechanics, and design of complex fluids; in particular, this includes yield stress fluids, polymer gels, biological materials, and largeamplitude oscillatory shear (LAOS) characterization. His work has been recognized by young investigator awards from NSF, ASME, 3M, DuPont, and The Society of Rheology.



Ewoldt R.H., Johnston M. T., Caretta L.M., "Experimental challenges of shear rheology: how to avoid bad data", in: S. Spagnolie (Editor), *Complex Fluids in Biological Systems*, Springer (2015) 1-36



What if I need help?

- •TA Tech Tips
 - http://www.youtube.com/tatechtips
- •On-site training & e-Training courses see Website
- TA Instruments Applications Helpline available from the TA website
 - http://www.tainstruments.com/support/applications/applicationshotline/
- Service related queries
 - Email: <u>servicehelpline@tainstruments.com</u>
 - Ph: 302-427-4050
- Check out our Website

<u>http://www.tainstruments.com/</u>

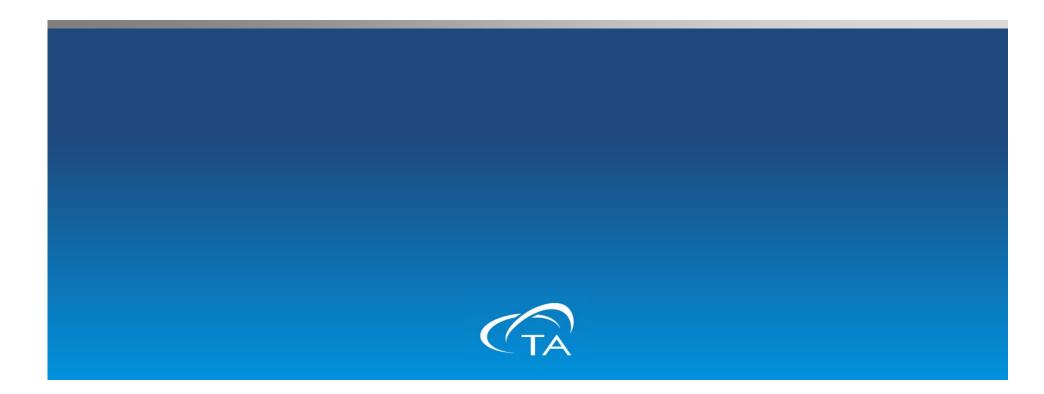


Thank You

The World Leader in Thermal Analysis, Rheology, and Microcalorimetry



Applications of Rheology Advanced Accessories



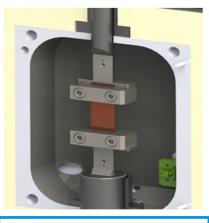
DHR Humidity Accessory





Bulk Diffusion





Film/fiber Tension

Temperature Range 5 ℃ - 120 ℃

Temperature Accuracy ±0.5 ℃

Heating/Cooling Rate ±1 °C/min maximum

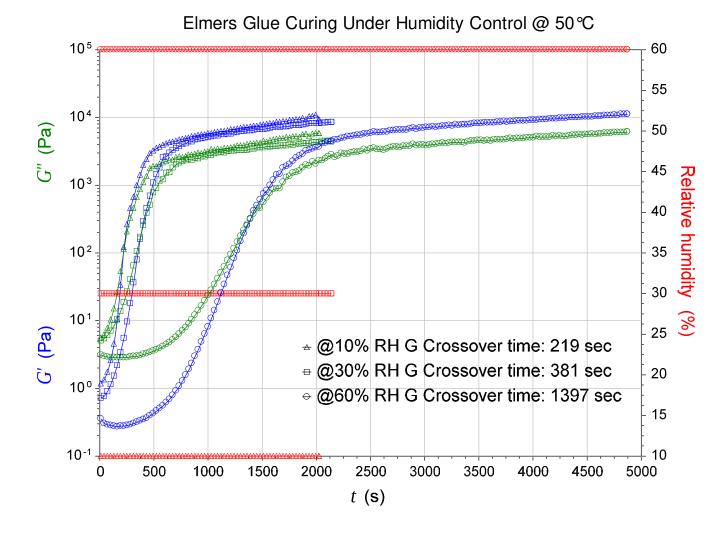
> Humidity Range 5- 95%

Humidity Accuracy 5-90%RH: ±3% RH >90%RH: ±5% RH

Humidity Ramp Rate ±2% RH/min increasing or decreasing



DHR Humidity Accessory



 Bulk diffusion geometry at 50°C and constant RH (10%, 30% and 60%)

 The test frequency -1.0 rad/s and oscillation torque -5 μN·m

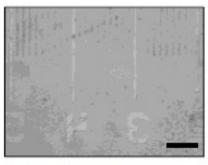




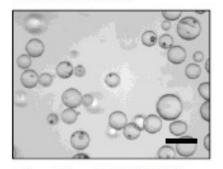
Modular Microscope Accessory (DHR)

 Connecting Rheology with structure under flow conditions (counter rotation option also available). Modular video camera, light source, and interchangeable optical objectives.

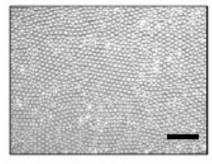




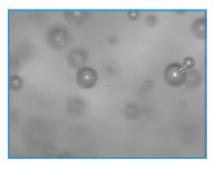
Calibration Grid, 20X



Glass Spheres in PDMS, 20X



7 µm Fluorescent PS Spheres, 20X



3D scan of hollow glass spheres, 20X



MagnetoRheology Accessory (DHR)

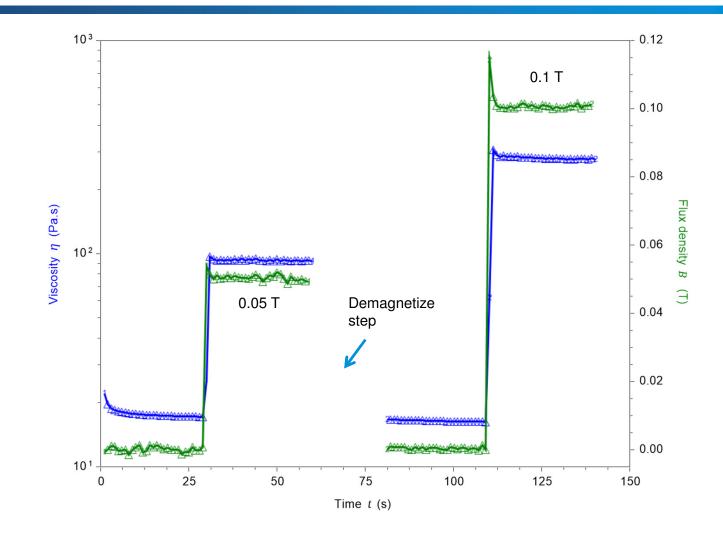
- The MR Accessory enables characterization of magneto-rheological fluids under the influence of a controlled field
- Applied fields up to 1 T with temperature range of -10 ℃ to 170 ℃ (standard and extended temperature options)
- The system accommodates an optional Hall probe for real-time measurement and closedloop control of the sample field







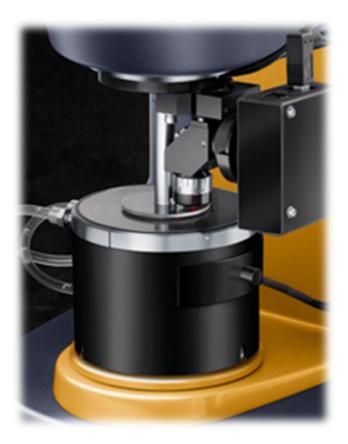
Magneto Rheology Accessory (DHR)



Lord MR Fluid MRF-140CG (081610) – 300µm gap at 20°C



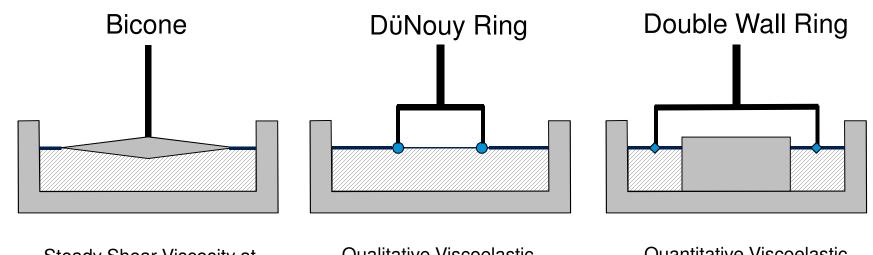
Small Angle Light Scattering (DHR)



- Simultaneous rheology and structure information
- Laser Light creates interference pattern
- Pattern reflects size, shape, orientation and arrangements of objects that scatter
- Objects scatter due to differences in refractive index



Interfacial Accessories



Steady Shear Viscosity at air/liquid and liquid/liquid interface.

Qualitative Viscoelastic measurements at air/liquid and liquid/liquid interface.

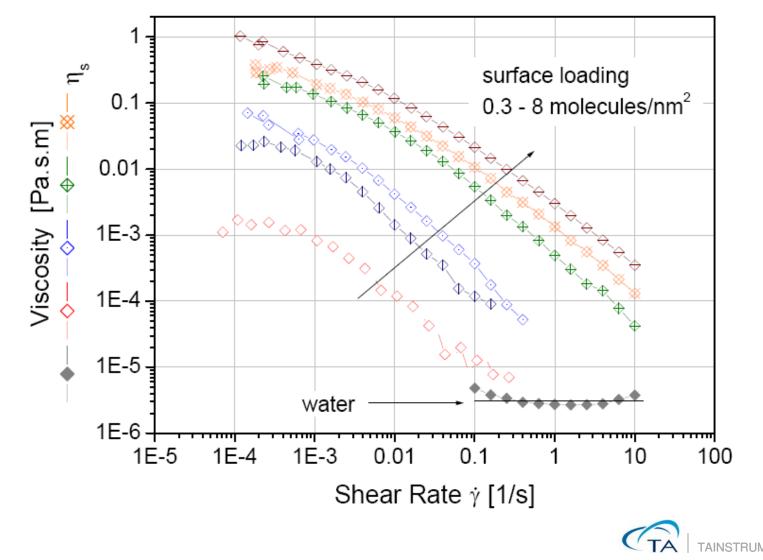
Quantitative Viscoelastic measurements at air/liquid and liquid/liquid interface.

- Interfacial shear rheology of thin layers at liquid-liquid or liquid-gas interfaces
- Effect of particles, surfactants or proteins at the interface
- Applications: food, biomedical, enhanced oil recovery



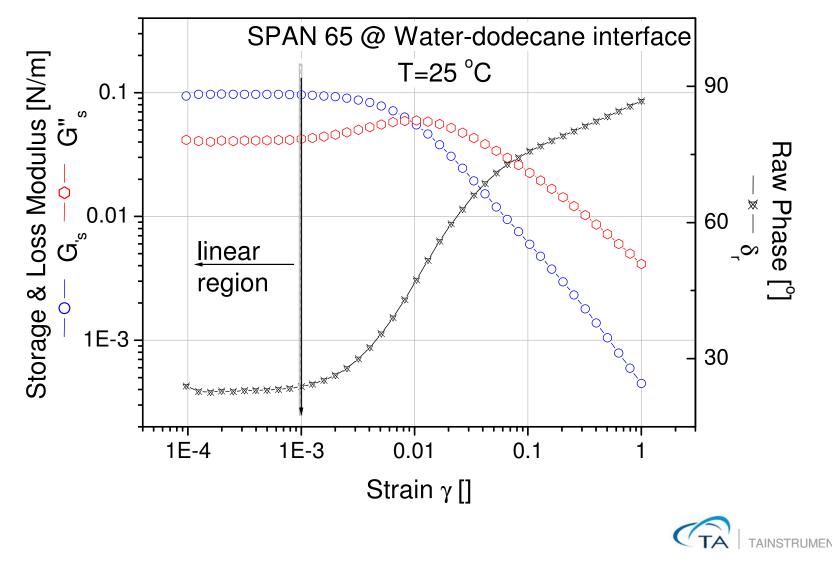
Surface Concentration Effects on Interfacial Viscosity

Surface viscosity of Span 65 layer deposited on water



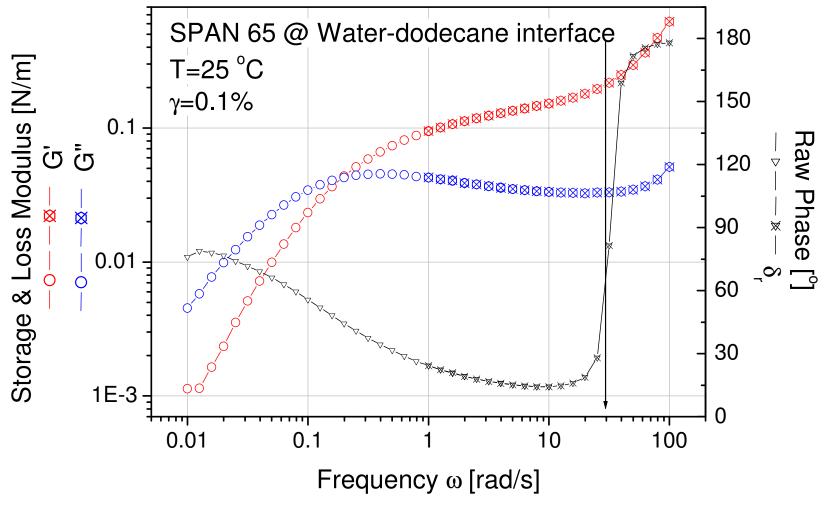
SPAN65® Water-Dodecane Interface

Interfacial properties Span65 @ water-dodecane interface

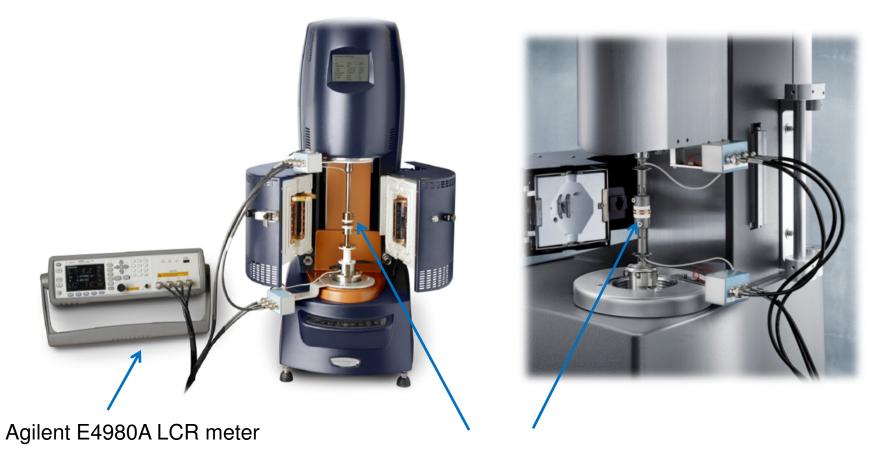


SPAN65® Water-Dodecane Interface

Interfacial properties Span65 @ water-dodecane interface



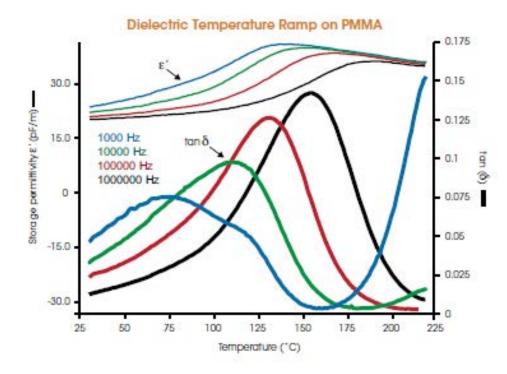
Dielectric Accessory



Ground Geometries with Ceramic Insulator (standard or disposable)



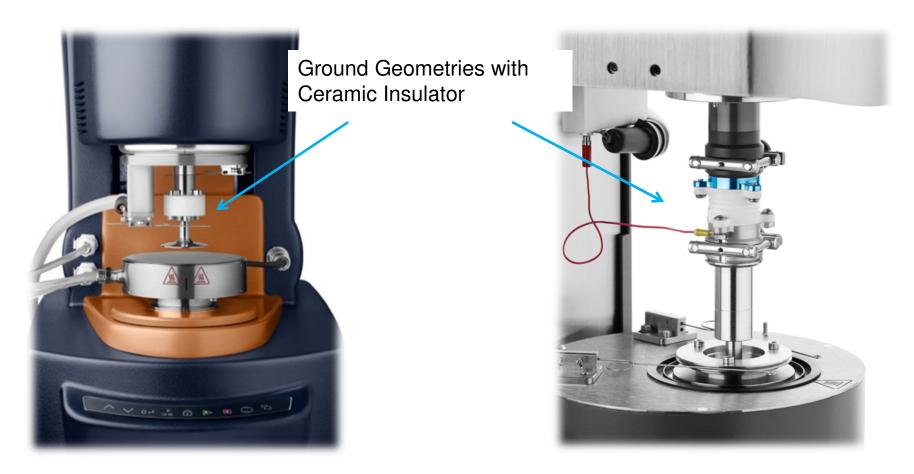
Dielectric Accessory



- Stand-alone or combined Dielectric-rheology
- LCR Fully programmable from TRIOS
- Wide temperature range: -160 to 350 ℃
- Applications: Characterize polar materials such as PVC, PVDF, PMMA, PVA



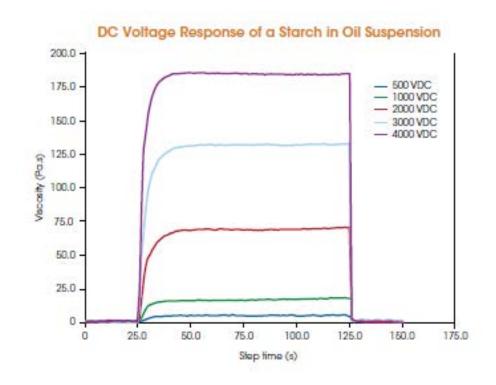
Electro-Rheology (ER) Accessory



Plates and DIN concentric cylinders



Electro-Rheology (ER) Accessory



•Wide range of voltage profiles

- Constant voltage
- Step voltage, ramp voltage
- Sine wave voltage function
- Triangle wave voltage function
- Wave functions with DC offsets
- Fully programmable from TRIOS

Applications:

- Hydraulic valves and clutches
- Shock absorbers
- Bulletproof vests
- Polishing slurries
- Flexible electronics



Peltier Plate Tribo-rheometry Geometries



Ball on three Plates



Three Balls on Plate



Ring on Plate

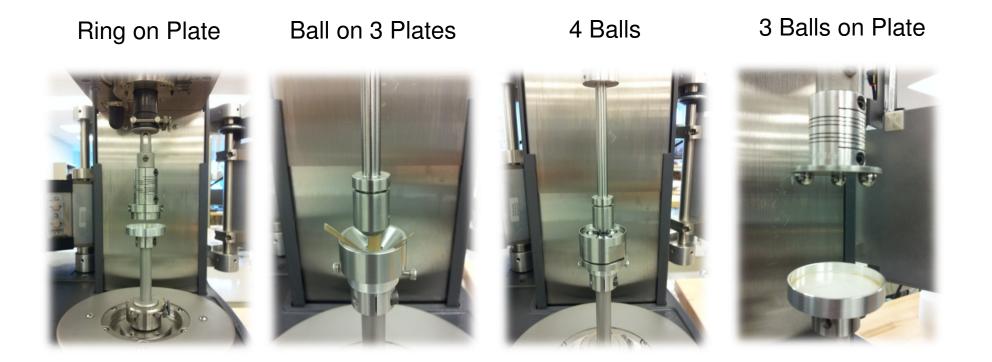


4 Balls





ARES G2 FCO and APS Tribology Accessory

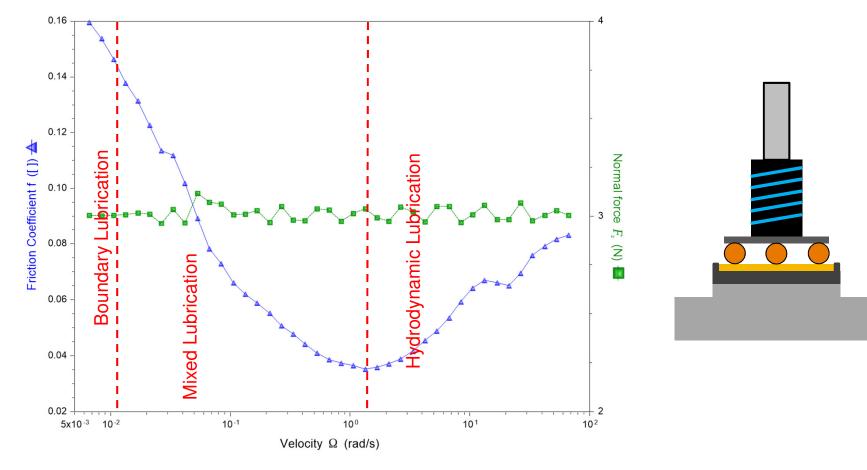


- High temperature with FCO
 - Applications: Automotive, High temp. greases/oils, Asphalt, Rubber
- Close to Room Temperature APS and Plate
 - Applications: Personal care products, Lubricants, Foods



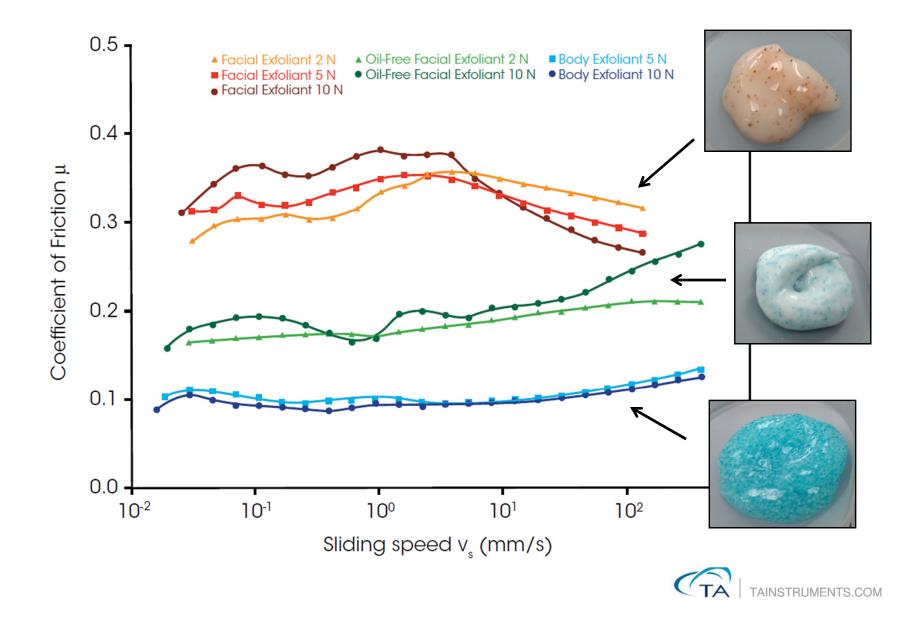
Coefficient of Friction Measurement

PVC on Steel with 2.0 Pa.s oil as lubricant Geometry: 3 Balls on Plate Temperature: 25 °C, Procedure: Flow ramp





Tribo-Rheometry: Exfoliants



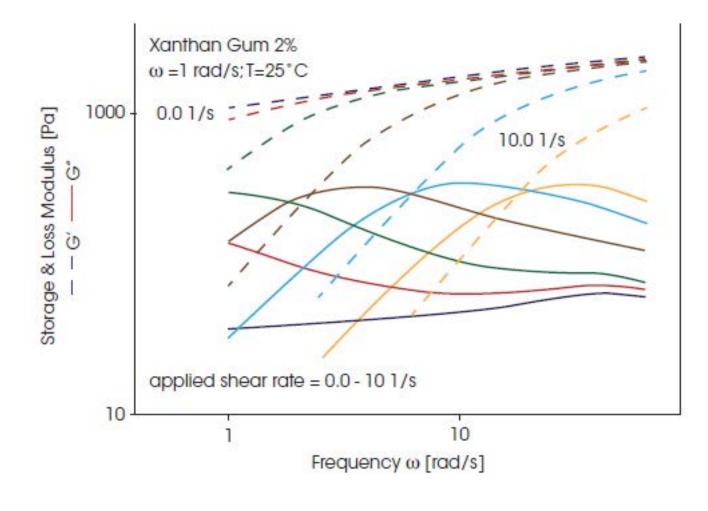
Orthogonal Superposition Features on ARES G2

- OSP on steady shear to monitor structural changes in materials (alternative to LAOS measurements)
- 2D-SAOS measurments to quantify anisotropy in materials
- Mentioned DMA capabilities previously in the polymer analysis section
- Simultaneous multiaxial testing of soft solids such as gels, foams, rubbers,...





Structure breakdown monitored by OSP



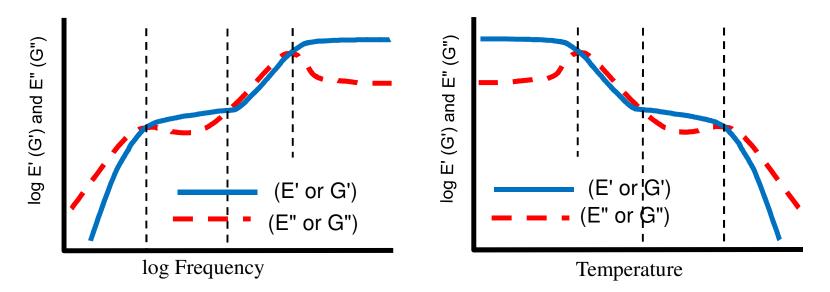
Steady shear breaks downs gel structure and moves flow region to shorter times scales (high frequencies)



Appendix 1: Time Temperature Superposition (TTS)



Time and Temperature Relationship



- Linear viscoelastic properties are both time-dependent and temperature-dependent
- Some materials show a time dependence that is proportional to the temperature dependence
 - Decreasing temperature has the same effect on viscoelastic properties as increasing the frequency
- For such materials, changes in temperature can be used to "re-scale" time, and predict behavior over time scales not easily measured



Time Temperature Superpositioning Benefits

- TTS can be used to extend the frequency beyond the instrument's range
- Creep TTS or Stress Relaxation TTS can predict behavior over longer times than can be practically measured
- Can be applied to amorphous, non modified polymers
- Material must be thermo-rheological simple
 - One in which all relaxations times shift with the same shift factor a_T



When Not to Use TTS

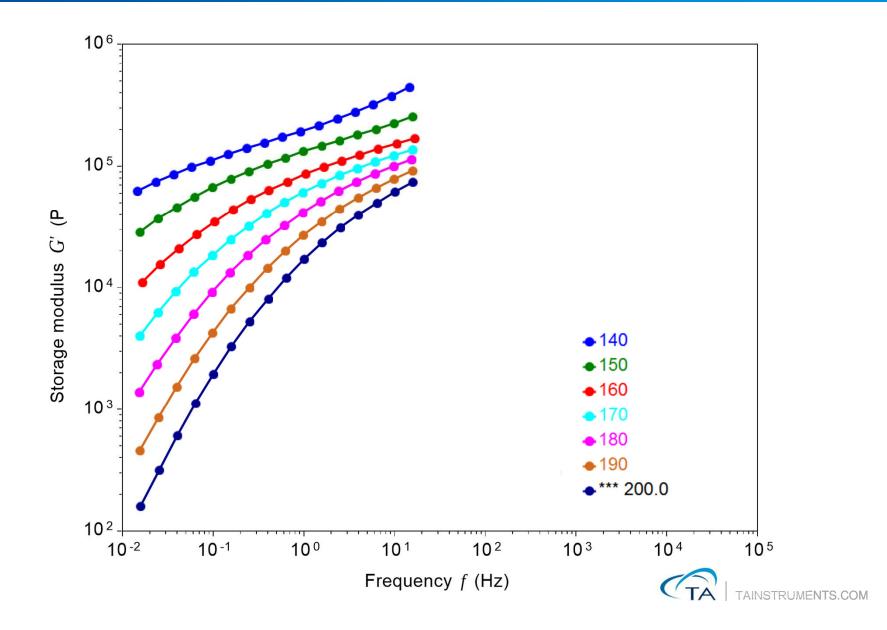
- If crystallinity is present, especially if any melting occurs in the temperature range of interest
- The structure changes with temperature
 - Cross linking, decomposition, etc.
 - Material is a block copolymer (TTS may work within a limited temperature range)
 - Material is a composite of different polymers
 - Viscoelastic mechanisms other than configuration changes of the polymer backbone
 - e.g. side-group motions, especially near the Tg
 - Dilute polymer solutions
 - Dispersions (wide frequency range)
 - Sol-gel transition

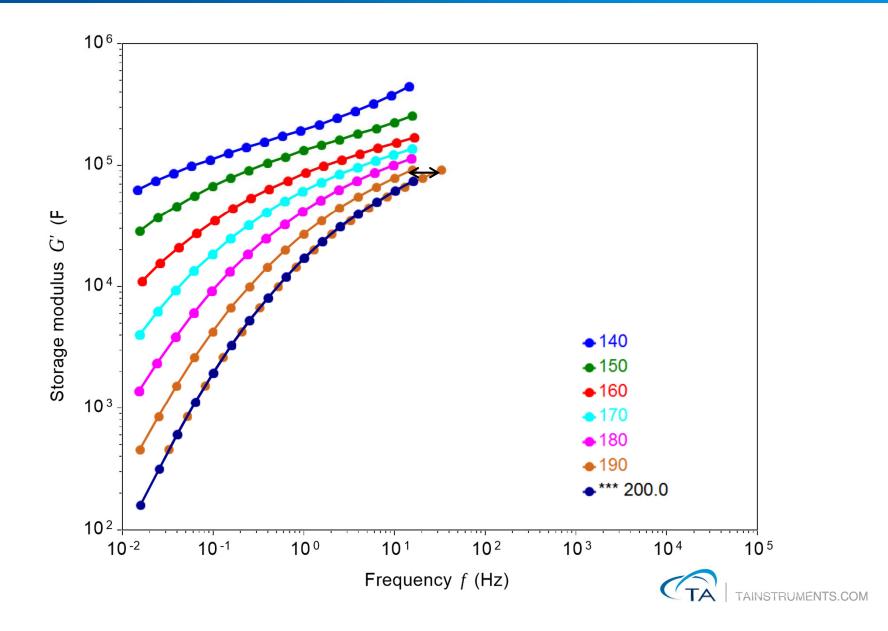


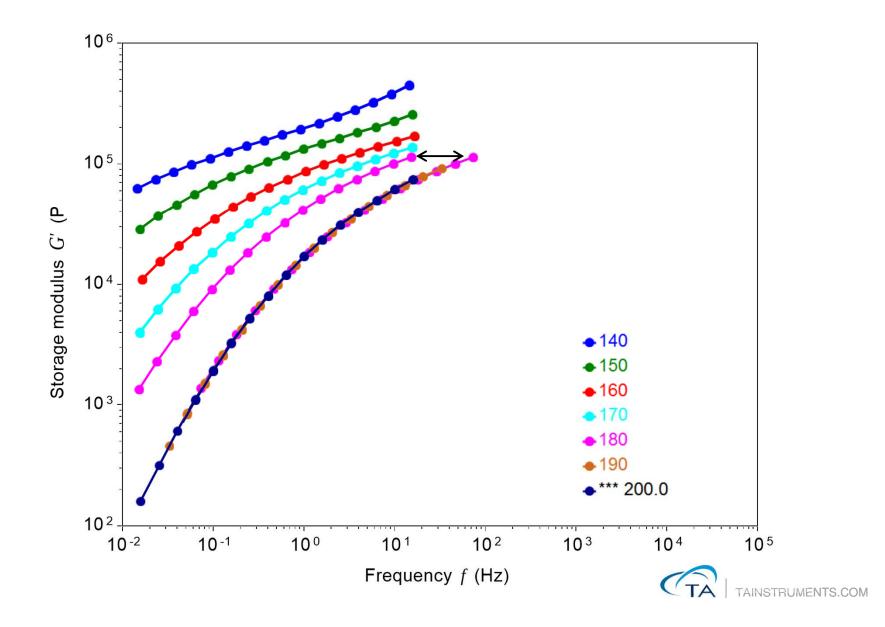
Guidelines for TTS

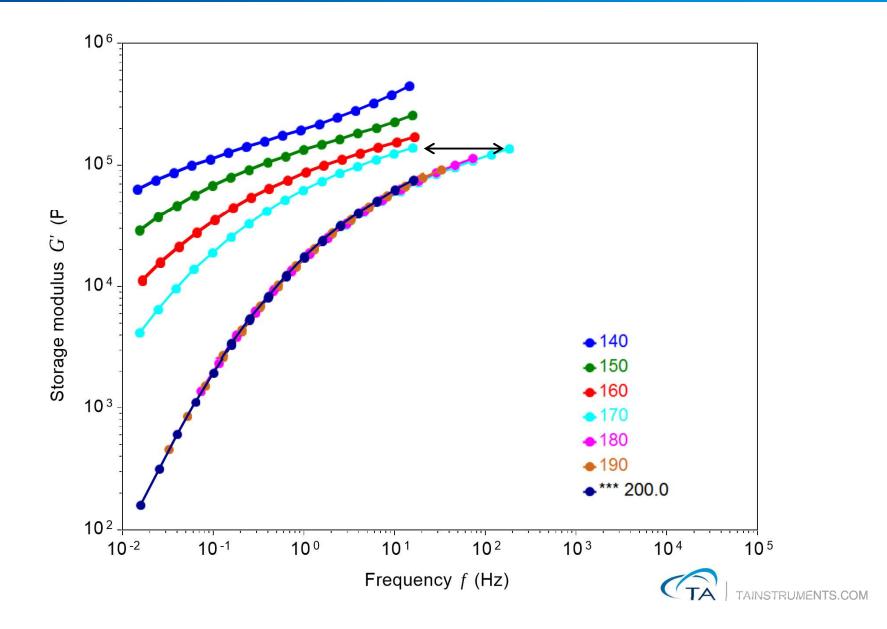
- Decide first on the Reference Temperature: T₀. What is the use temperature?
- If you want to obtain information at higher frequencies or shorter times, you will need to conduct frequency (stress relaxation or creep) scans at temperatures lower than T₀.
- If you want to obtain information at lower frequencies or longer times, you will need to test at temperatures higher than T₀.
- Good idea to scan material over temperature range at single frequency to get an idea of modulus-temperature and transition behavior.

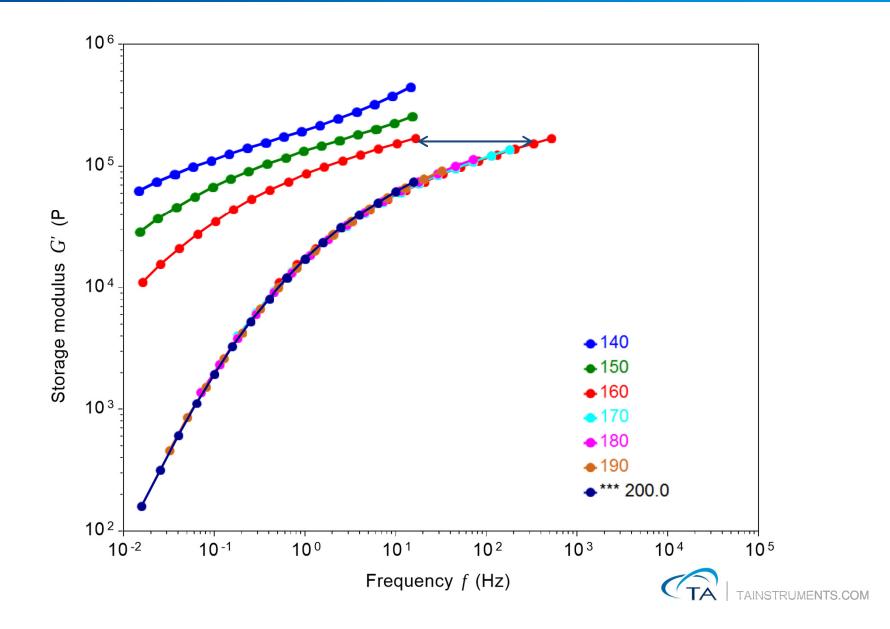


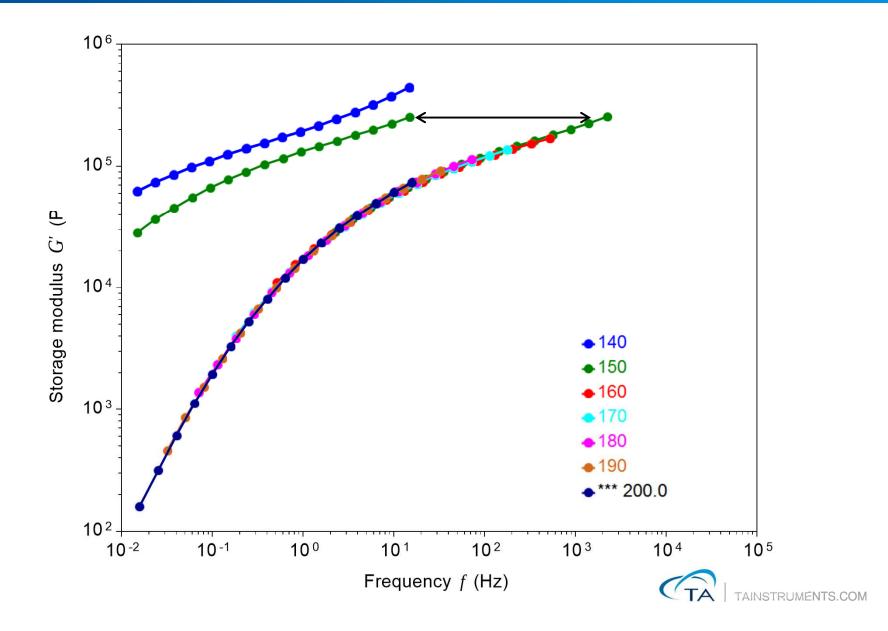


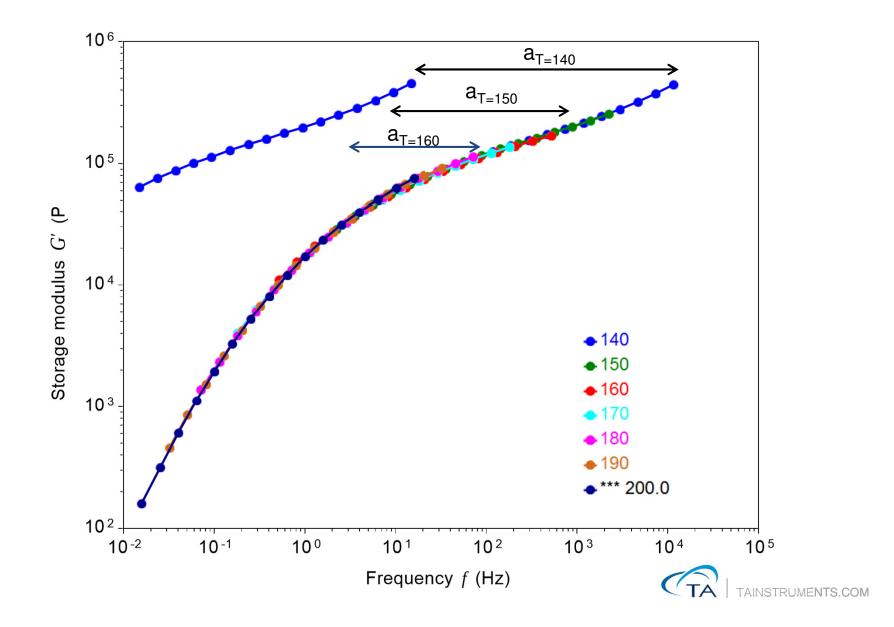




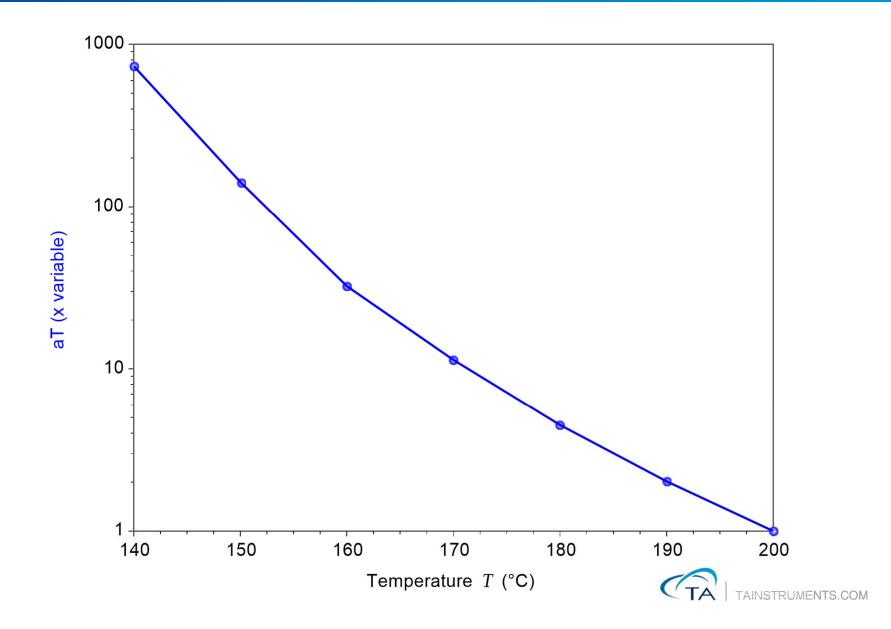








Shift Factors a_T vs Temperature



Shift Factors: WLF Equation

 Master Curves can be generated using shift factors derived from the Williams, Landel, Ferry (WLF) equation

 $\log a_{T} = -c_{1}(T-T_{0})/c_{2} + (T-T_{0})$

- a_T = temperature shift factor
- T_0 = reference temperature
- c_1 and c_2 = constants from curve fitting
 - Generally, $c_1 = 17.44 \& c_2 = 51.6$ when $T_0 = T_g$



When not to use the WLF Equation

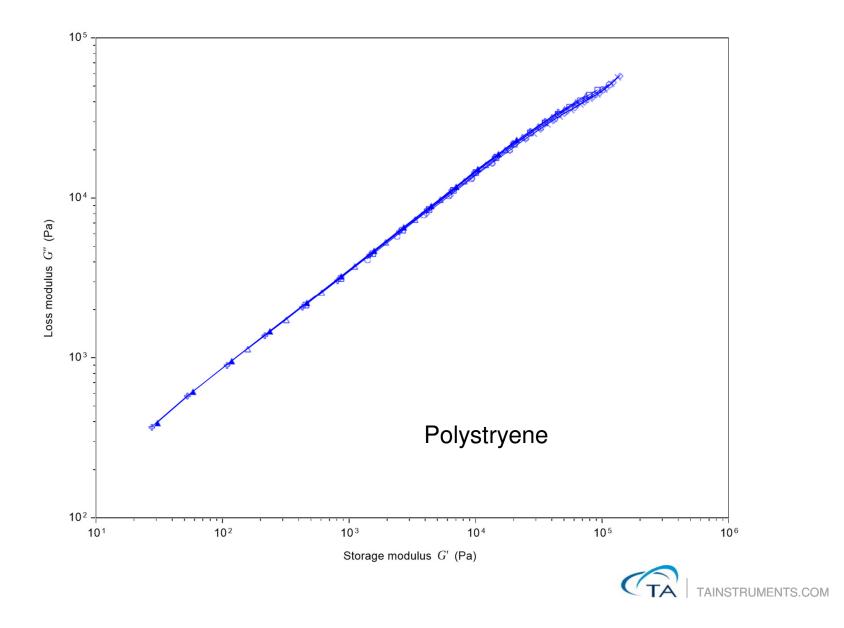
- Sometimes you shouldn't use the WLF equation (even if it appears to work)
- If T > T_g+100 ℃
- If $T < T_g^{o}$ and polymer is not elastomeric
- If temperature range is small, then $c_1 \& c_2$ cannot be calculated precisely
- In these cases, the Arrhenius form is usually better

 $\ln a_{T} = (E_{a}/R)(1/T-1/T_{0})$

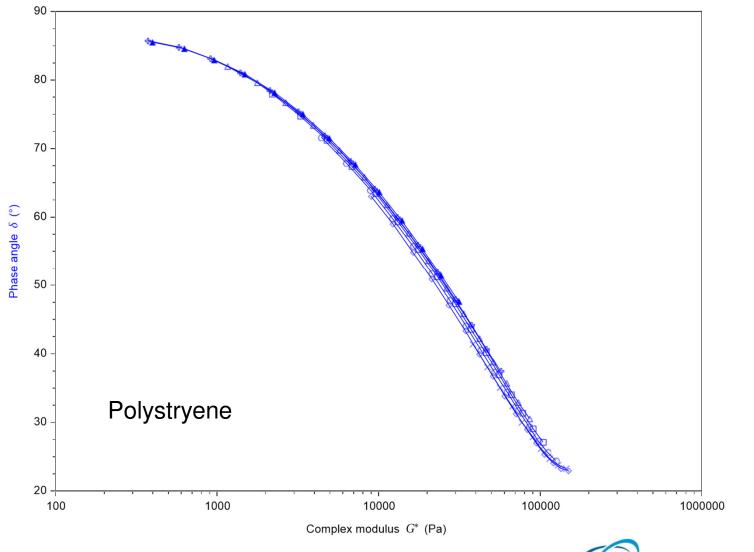
- a_T = temperature shift factor
- $E_a = Apparent activation energy$
- T_0 = reference temperature
- T = absolute temperature
- R = gas constant
- $E_a = activation energy$



Verify Data for TTS



Verify Data for TTS





References for TTS

- 1) Ward, I.M. and Hadley, D.W., "*Mechanical Properties of Solid Polymers*", Wiley, 1993, Chapter 6.
- 2) Ferry, J.D., "Viscoelastic Properties of Polymers", Wiley, 1970, Chapter 11.
- 3) Plazek, D.J., "*Oh, Thermorheological Simplicity, wherefore art thou?*" Journal of Rheology, vol 40, 1996, p987.
- 4) Lesueur, D., Gerard, J-F., Claudy, P., Letoffe, J-M. and Planche, D., "*A structure related model to describe asphalt linear viscoelasticity*", Journal of Rheology, vol 40, 1996, p813.

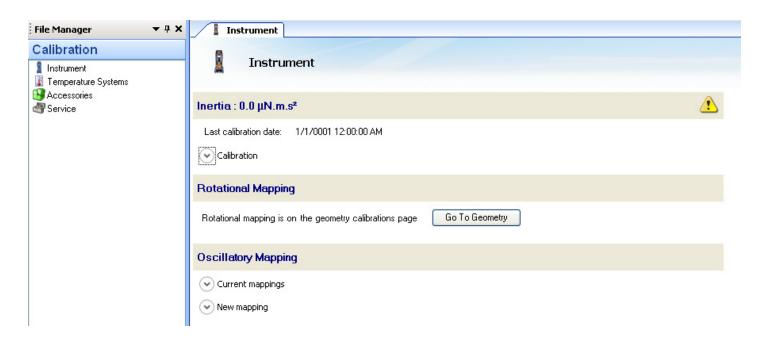


Appendix 2: Rheometer Calibrations DHR and AR



DHR – Calibration Options

- Instrument Calibrations
 - Inertia (Service)
 - Rotational Mapping
 - Oscillation Mapping (recommended for interfacial measurements)





DHR – Inertia Calibration

- Go to the Calibration tab and select Instrument
 - Make sure there is no geometry installed and then click calibrate

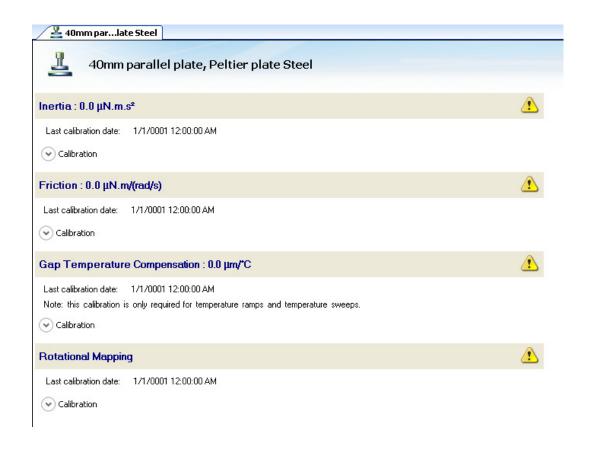
Experiments	File Manager 🔷 🔻 🛪	
Results Geometries Calibration	Calibration	
Instrument		
Inertia : 21.0325 µN.m.s ²		~
Last calibration date: 11/15/2011 7:36:14 AM		
Before calibration Please ensure that no geometry is attached a	and that the spindle is free to rotate.	
Calibration will take 30 seconds	Calibrate Accept Cancel	



DHR – Geometry Calibration

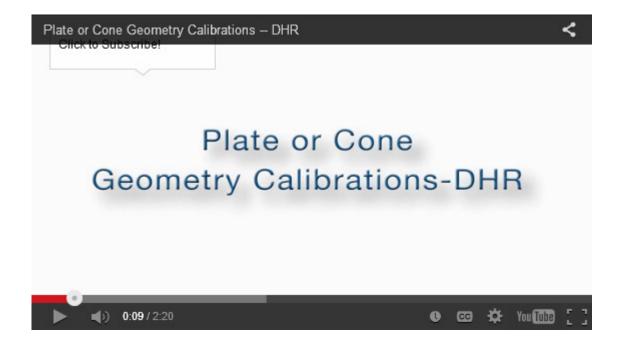
- Geometry Calibrations:

- Inertia
- Friction
- Gap Temperature Compensation
- Rotational Mapping





TA Tech Tip – Geometry Calibrations



 Videos available at <u>www.tainstruments.com</u> under the Videos tab or on the TA tech tip channel of YouTube[™] (<u>http://www.youtube.com/user/TATechTips</u>)

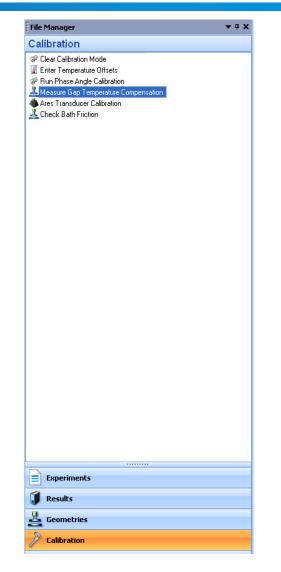


Appendix 2: Rheometer Calibrations ARES-G2



ARES-G2 – Calibration Options

- Instrument Calibrations
 - Temperature Offsets
 - Phase Angle (Service)
 - Measure Gap Temperature Compensation
 - Transducer
- Geometry Calibrations:
 - Compliance and Inertia (from table)
 - Gap Temperature Compensation





ARES-G2 – Transducer Calibration

1.000			Transducer Calibration Procedure		
			Torque O Normal	Force	
1)	Torque Calibration		
	P		1. Install the calibration fixture and p	pully (without weigh	nt)
		1	2. Zero Torque Transducer	Zero	
	>		3. Hang weight from the pulley		
			Calibration mass	500.000	g
		Å	Moment arm length	2.50000	cm
	6	5	Applied Torque	1250.00] g cm
			4. Measure resulting torque	Measure	
			New calibration factor	0.00000] g cm
			Abort	Apply	
Transducer	0.700			0100.05	1 2240
Torque	-0.720	gcm	Torque calibration factor	2106.05	gcm
Normal Force	-53.202	g	Normal force calibration factor	2090.05	g



ARES-G2 – Geometry Calibration

* Geometry: 40mm parallel plate,	Stainless ste	el		
Diameter40Gap1.0Loading gap10.0Trim gap offset0.05	mm mm mm mm			
Material Stainless steel Minimum sample volume is 1.2 Constants		~	/ •	Gap Tem Enter r
Gap temperature compensation Expansion coefficient Move stage to maintain star Upper compliance	0.0	µm/°C mrad/N.m	•	Compliar (from t
Lower compliance Geometry inertia	0.0	mrad/N.m		- (1101111
Stress constant	79577.5	Pa/N.m		Geometr
Strain constant Stress constant (linear)	20.0 795.775	1/rad Pa/N ←		 Calcula
Strain constant (linear) Normal stress constant	1000.0 1591.55	1/m Pa/N		

- Gap Temperature Compensation
 - Enter manually or run calibration
- Compliance and Inertia
 - (from table in Help menu)
- Geometry Constants
 - Calculated based on dimensions



Geometry Inertia & Compliance- Help Menu

• Click here for a spreadsheet that contains the inertia, compliance, and gap compensation data for the majority of the ARES-G2/ARES tooling.

🕗 🥙 C:\Program Files (x	&6)\TA Instruments\TRIOS\He	elp\ARESG2\TRIOS_Help_AF	R の -	Online Help ×						ሰ 🕁
Search		<u>8</u> 24								TRIOS
Ce Search ()	ARES-G Click on column header Enter Text in box above		etries							
S-G2 Test Geometri es ARES-G2 Rheomet	Catalog Number	Part Number	Size (mm)	Туре	Additional Features	Usage (ARES Classic or ARES-G2)	Material	Window Style	Inertia µN*m*s²	Compliance mrad/N*m
er: Setting Up a Ste p (Transient) Creep				Cone						
Test Inertia and Complia	708.01002.1	401.00536.1	25mm	Cone	.02 radian .100" dia tip	Both	SST 316	Rectangular	3.59E+00	2.67E+00
nce Correction Loading ARES-G2	708.01002.10	401.00536.10	25mm	Cone	.10 radian .040" dia tip	Both	INVAR-36	Rectangular	3.60E+00	3.57E+00
Samples		401.00536.11	25mm	Cone	.10 radian .040" dia tip	Both	SST 17-4PH	Rectangular	3.47E+00	2.63E+00
Configuring a New Geometry		401.00536.12	25mm	Cone	.10 radian .040" dia tip	Both	TITANIUM 6AL-4V	Rectangular	1.98E+00	4.75E+00
Understanding the Variables		401.00536.13	25mm	Cone	.02 radian .236" dia tip	Both	TITANIUM 6AL-4V	Rectangular	1.98E+00	4.75E+00
Calculating Drift Cor		401.00536.14	25mm	Cone	.04 radian .236" dia tip	Both	TITANIUM 6AL-4V	Rectangular	1.98E+00	4.75E+00
rection for Recover able Compliance		401.00536.15	25mm	Cone	.01 radian .157" dia tip	Both	TITANIUM 6AL-4V	Rectangular	1.98E+00	4.75E+00
Transformations		401.00536.16	25mm	Cone	.10 radian .040" dia tip	Both	HASTELLOY-B2	Rectangular	4.23E+00	2.49E+00
Operating the Diele ctric Accessory	708.01002.17	401.00536.17	25mm	Cone	.01 radian .157" dia tip	Both	SST 316	Rectangular	3.59E+00	2.67E+00
About the TRIOS G uardian™ Option		401.00536.2	25mm	Cone	.02 radian .100" dia tip	Both	INVAR-36	Rectangular	3.60E+00	3.57E+00
Discrete Retardatio n Time Spectrum		401.00536.3	25mm	Cone	.02 radian .100" dia tip	Both	SST 17-4PH	Rectangular	3.47E+00	2.63E+00
Setting Up an Oscill		401.00536.4	25mm	Cone	02 radian 100" dia tin	Both	TITANIUM 6AI -4V	Rectangular	1.98E+00	4 75E+00

What if the online table does not list a compliance value for my specific geometry? Use the compliance value for a geometry of the same/similar dimension, type, and material.



ARES-G2 - Gap Temperature Compensation

• • • • • • • • • • • • • • • • • • •	dap remperatu	are Compensation Calibration	۱ <u> </u>	
New Expansion Coefficient µm/*C Commit Temperature / Time Profile ● Run at Gap ● Maintain Zero Gap Maintain Force 5.0 N Starting Temperature -80 °C Start Temperature Equilibration Time 300 s ● Ramp Temperature © Step Temperature Temperature Ramp Rate 1.0 °C/min Final Temperature 65 °C	Geomety Name	40mm parallel plate, Stain	nless steel	
New Expansion Coefficient µm/*C Commit Commit Temperature / Time Profile Commit Image: Start Gap Maintain Zero Gap Maintain Force 5.0 N Starting Temperature -80 °C Start Temperature Equilibration Time 300 s Image: Ramp Temperature Step Temperature Temperature Temperature Ramp Rate 1.0 °C/min Final Temperature 65 °C	Notes			
 Run at Gap Maintain Zero Gap Maintain Force Starting Temperature Start Temperature Equilibration Time 300 Samp Temperature Step Temperature Temperature Ramp Rate 1.0 °C 		-		
Starting Temperature -80 °C Start Temperature Equilibration Time 300 s Start Temperature Equilibration Time 300 s Start Temperature Equilibration Time 300 s Temperature Ramp Rate 1.0 °C/min Final Temperature 65 °C		Time Profile		
Start Temperature Equilibration Time 300 s Start Temperature Equilibration Time 300 s Ramp Temperature Step Temperature Temperature Temperature Ramp Rate 1.0 °C/min Final Temperature 65 °C			Zero Gap	
 Ramp Temperature Step Temperature Temperature Ramp Rate 1.0 °C/min Final Temperature 65 °C 	🔿 Run at	Gap 💿 Maintain		N
Temperature Ramp Rate 1.0 °C/min Final Temperature 65 °C	◯ Run at Maintain Fi	:Gap 💿 Maintain. orce	5.0	
Final Temperature 65 °C	◯ Run at Maintain F Starting Te	Gap Maintain roce mperature	-80	°C
	Run at Maintain Fu Starting Te Start Temp	Gap	5.0 -80 300	°C
Final Temperature Equilibration Time 300 s	Run at Maintain For Starting Te Start Temp Ramp	Gap	5.0 -80 300	°C s
	Run at Maintain Fu Starting Te Start Temp Ramp Temperatu	Gap	5.0 -80 300 mperature 1.0	°C s °C/min



General Rheometer Maintenance

- Air Supply
 - Dry particulate-free air (dew point -40 °C)
 - Check filters/regulators on a periodic basis to ensure proper pressure, free of moisture/oil/dirt buildup.
 - If air must be turned off, then make sure that the bearing lock is fastened
 - NOTE: Do not rotate drive-shaft if air supply is OFF!
- Location
 - Isolate the instrument from vibrations with a marble table or Sorbathane pads.
 - Drafts from fume hoods or HVAC systems and vibrations from adjacent equipment can contribute noise to measurements, particularly in the low torque regime. Use a Draft Shield to isolate instrument from drafts.



General Rheometer Maintenance - Peltier

Circulator Maintenance

- Proper operation of a fluid circulator is vital for correct and efficient operation of Peltier-based temperature control devices.
- Check fluid levels and add anti-fungal additive regularly.
 - Note: if operating circulator below 5°C then it is recommended to fill the circulator with a mixture or material with a lower freezing point than water to prevent permanent circulator damage.
 - Example: add ~20% v/v ethanol to water
- Keep it clean!
 - Flush and clean circulator, Peltier system, and tubing at first sight of contamination.
 - When not in use, it is strongly recommended to deactivate the Peltier device and turn off the circulator.





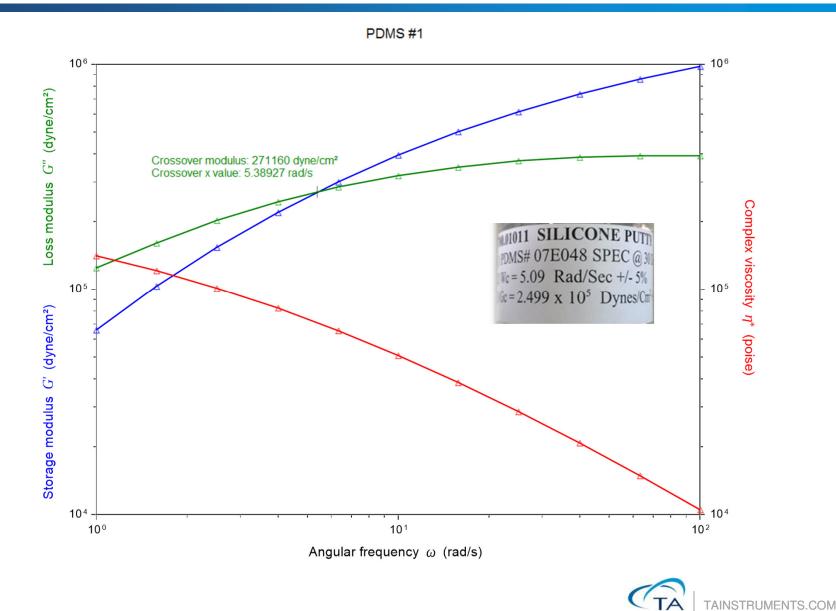


Verify Rheometer Performance

- Rheometers are calibrated from the factory and again at installation.
- TA recommends routine validation or confidence checks using standard oils or Polydimethylsiloxane (PDMS).
- PDMS is verified using a 25 mm parallel plate.
 - Oscillation Frequency Sweep: 1 to 100 rad/s with 5% strain at 30°C
 - Verify modulus and frequency values at crossover
- Standard silicone oils can be verified using cone, plate or concentric cylinder configurations.
 - Flow Ramp: 0 to 88 Pa at 25°C using a 60 mm 2° cone
 - Service performs this test at installation



PDMS Frequency Sweep Results



Load Standard Oil

- Set Peltier temperature to 25°C and equilibrate.
 - Zero the geometry gap
- Load sample
 - Be careful not to introduce air bubbles!
- Set the gap to the trim gap
- Lock the head and trim with non-absorbent tool
 - Important to allow time for temperature equilibration.
- Go to geometry gap and initiate the experiment.







Flow Ramp – Standard Oil (Service Test)



